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# **USAAMRDL TECHNICAL REPORT 71-58**

# CH-47A, B AND C SERIES HELICOPTER ROTOR BLADE FAILURE AND SCRAP RATE DATA ANALYSIS

By R. L. Hunt

November 1971

NATIONAL TECHNICAL INFORMATION SERVICE Springfield, Va. 22151

# U. S. ARMY AIR MOBILITY RESEARCH AND DEVELOPMENT LABORATORY FORT EUSTIS, VIRGINIA

CONTRACT DAAJ02-71-C-0014
THE BOEING COMPANY, VERTOL DIVISION
PHILADELPHIA, PENNSYLVANIA

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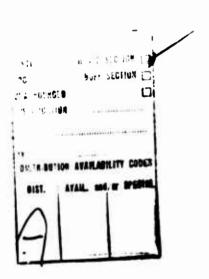
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rotor blades of the CH-47 series ta	ndem rotor	helicon	ters. Two types		
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mean-time-between-scrappage. Locat					
discrepancies were determined. Bla					
A cost comparison of blade acquisit					
of repair/rework was provided.					

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# DEPARTMENT OF THE ARMY U. S. ARMY AIR MOBILITY RESEARCH & DEVELOPMENT LABORATORY EUSTIS DIRECTORATE FORT EUSTIS, VIRGINIA 23604

The Eustis Directorate of the U.S. Army Air Mobility Research and Development Laboratory is conducting a series of design studies and hardware evaluations leading to improved reliability and maintainability (R&M) characteristics for future helicopter rotor blades. It is intended that design requirements will be tailored to each aircraft type (utility, attack, transport, etc.) with full consideration of operational environment impacts (combat damage, foreign object damage, etc.) included.

This contract was awarded to analyze the operational R&M history of CH-47A, B, and C model helicopter rotor blades to establish design considerations for transport type aircraft. The findings presented herein are considered to be most accurate and directly usable in establishing expected rotor blade external damage rates for the type of helicopter in question. Results of this analysis will be used for evaluation of advanced rotor blade design concepts currently being investigated under this Directorate's R&M research and development program. This report is published as a parallel to the USAAVLABS Technical Report 71-9, "UH-1 and AH-1 Helicopter Main Rotor Blade Failure and Scrap Rate Data Analysis", which presented data for consideration in the design of utility and attack helicopter rotor blades.

The technical monitor for this contract was Major Vincent G. Ripoll, Reliability and Maintainability Division, Eustis Directorate.

### Task 1F162205A11901 Contract DAAJ02-71-C-0014 USAAMRDL Technical Report 71-58 November 1971

CH-47A, B AND C SERIES HELICOPTER ROTOR BLADE FAILURE AND SCRAP RATE DATA ANALYSIS

Final Report D210-10340-1

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U.S. ARMY AIR MOBILITY RESEARCH AND DEVELOPMENT LABORATORY
FORT EUSTIS, VIRGINIA

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### SUMMARY

This report has the purpose of providing the results of an analysis of failure data derived from depot inspection, overhaul/rework, and scrappage of 5,488 rotor blades of the CH-47 series tandem rotor helicopters. These blades were returned after RVN and CONUS operations over a time period from July 1, 1962 through March 1, 1971, with an accumulation of 2,521,734 actual blade operating hours with an equivalent accumulation of 5,679,399 operating hours for all blades in the helicopter fleet.

Analyses of unscheduled removals, repair, overhaul, and scrap data were conducted on two different types of blades. Compilation of total quantity of blades investigated has been provided, as well as accumulated time on all blades at removal.

Analyses to determine the blade design parameters as mean-time-between-removals (MTBR), mean-time-to-removals (MTTR) and mean-time-between-unscheduled-removals (MTBUR) have been included. Results may be compared for changes in these parameters in preceding from the early to the later model. Changes in these parameters can be attributed to incorporation of engineering changes, evolution of improved manufacturing, shipping, handling and modified maintenance practices.

Analyses to determine reasons for removals, repairs and scrappage as a percentage of total blades removed and of total blades scrapped have been compiled. Reported reasons for removal are consistent with reasons for repair and for scrappage. Blades subjected at the manufacturer's repair facility to close detailed inspection, disassembly, or repair for minor damage sometimes indicated serious defects as extensive water migration, exterior spar corrosion and similarly hidden damages. Additional reasons for scrappage were, therefore, discovered. A very minor quantity of blades may be scrapped due to in-transit depot handling and processing damages. Analysis results for the mean-time-between-scrappage (MTBS) for both CH-47A and B/C blades have been included.

Conclusions of this analysis indicate that the later CH-47B/C blades have been designed to decrease the amount of inherent discrepancies. However, they are more susceptible to externally caused discrepancies than the CH-47A helicopter blades. It is recommended that field repair and blade handling procedures be reviewed for modifications in line with the results of this report.

### FOREWORD

This report provides an analysis of rotor blade failure and scrap rate historical data as reported on the tandem rotor helicopters, CH-47A, CH-47B and CH-47C. This analysis was conducted under Contract DAAJ02-71-C-0014 (Task 1F162205A11901) for the Eustis Directorate, U. S. Army Air Mobility Research and Development Laboratory (USAAMRDL), Fort Eustis, Virginia.

USAAMRDL technical direction was provided by Major Vincent G. Ripoll.

The principal analyst for The Boeing Company, Vertol Division, was Mr. R. L. Hunt, assisted by Mr. E. C. Daley and Mr. J. J. Chmura, all of M&R Engineering. Program management and technical direction were provided by Mr. H. J. Smith, Sr., Product Support Engineer, Mr. R. E. Spears, Sr., Product Support Engineer, Mr. R. Hazlett, Manager Product Assurance R&D, and Mr. P. W. Fiedler, Unit Chief Reliability and Maintainability.

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### INTRODUCTION

Helicopter rotor blade failure and scrap rate information as reported during depot rework is an important source of blade data. This data may be used analytically to determine removal rates and mean removal values, to determine blade scrappage rates and mean scrappage values and enable correlation of these rates and values with the various reasons for blade removal from the helicopter and for subsequent repair or scrappage.

The above data was available, as The Boeing Company, Vertol Division has been repairing and updating CH-47 helicopter rotor blades under a U. S. Army contract since the incorporation of this helicopter into the Army inventory in 1962.

During the time from 1962 through 1970, the Vertol Division has been the sole contractor for depot rework of CH-47 helicopter rotor blades. From all data generated from the rework facility and from field activities, a data system was developed to record utilization, discrepancies, failure modes, configuration control, and reason for blade removal/scrappage. This data has been maintained in a usable format to enable blade analyses to be readily accomplished at any time.

This data has been continually extracted, reviewed and verified by Boeing Company/Vertol Division personnel who possessed specialized backgrounds in the fields of reliability, maintainability, service engineering, design, military/aviation, data analysis and military/civilian overhaul/repair facilities. It is from the above data source that this CH-47A, B and C series helicopter rotor blade failure data and scrap rate data analysis has been compiled.

### SCOPE

The objective of this effort was to conduct an analysis of available CH-47A, B and C series helicopter rotor blade failure and scrap rate data to determine unscheduled and scheduled removal rates, to develop mean-time-between-removal values, to determine blade scrappage rates, and to correlate these rates and values with the various reasons for removal and scrappage.

This data was derived entirely from depot level repair and scrappage reports on two types of rotor blades used on three different helicopter models as shown by Table I below.

TABLE I. ANALYZED ROTOR BLADES IDENTIFICATION				
APPLICABLE HELICOPTER	HELICOPTER SERIAL NUMBERS	APPLICABLE ROTOR BLADES PART NUMBERS		
CH-47A	59-4982 & Subsequent	P/N 114R1002		
CH-47B	66-19098 & Subsequent	P/N 114R1502		
CH-47C	67-18494 & Subsequent	P/N 114R1502		

The CH-47A type of rotor blade with a steel spar, fiberglass skins, and aluminum ribs is constructed as a symmetrical airfoil. The CH-47B/C type of rotor blade, with a steel spar, fiberglass skins, honeycomb fillers and plastic end ribs is constructed as a nonsymmetrical airfoil. Due to these major design differences, the analytical effort, therefore, treated these two types of blades independently. A detailed discussion of blade differences and how these were treated in the analyses is given under analysis approach, page 3.

### ANALYSIS APPROACH

This section describes the preliminary steps taken prior to accomplishment of the analytical efforts concerned with blade removals and blade scrappage.

The two types of blade configurations, i.e., CH-47A symmetrical type and the CH-47B/C nonsymmetrical type, and their different installation locations, i.e., forward and aft rotors, have had a bearing upon the extent of data available for extraction; therefore, these blade configurations and installations are described in detail herein.

The organization of the data into a form suitable for extraction of material useful for the analyses contained in this report required the application of a specific data extraction process which is discussed below.

Certain data limitations exist for the data reporting time period investigated. One limitation concerns the fact that all blade repairs, overhaul, and scrappage have been accomplished at the depot level. Thus data reporting on blade repairs and scrappage occurred at this level for a total of 2,521,734 actual blade hours. During this same interval, if field level (organizational through general support maintenance levels) data had been available, a total of 5,679,399 blade operating hours could have been used as the analysis data base. A second limitation is the possible loss of data due to unusual incidents. A third limitation is the possible dilution of the blade population by excessive categorization. These limitations are discussed herein.

Identification of reasons for removal, repair, and scrappage required a simplified tabulation of the standard military coding to handle the quantity of data. This tabulation is discussed below. Recognition of the inspection criterion against which blades are removed or scrapped is discussed.

Calculation of blade means representative of blade operating experience requires definition of these means and development of appropriate equations. These steps are presented herein.

### DESCRIPTION OF CH-47 HELICOPTER ROTOR SYSTEMS

### CH-47A Rotor Systems

The CH-47A helicopter rotor system consists of two rotor installations: one at the forward end of the aircraft and one at the aft end, as shown in Figure 1. These installations are similar but not identical. Each installation includes three interchangeable blade assemblies and a rotor head assembly. The helicopter thus has a total of six blades. These blades are not interchangeable between the two locations. Blade rotation direction is counterclockwise for the forward rotor and clockwise for the aft rotor (in a plan view).

### CH-47B/C Rotor Systems

The CH-47B/C rotor system is similar to that of the CH-47A. However, the blades used on these two types of aircraft are different and are not interchangeable between aircraft.

### DESCRIPTION OF CH-47 HELICOPTER ROTOR BLADES

### CH-47A Rotor Blades

The CH-47A rotor blade assembly as shown in Figure 2 is a symmetrical airfoil shape. It consists of a D-spar, an attaching socket, a nose cap assembly, a trailing-edge strip, twelve boxed fairings, tip balance provisions, and a faired tip cover. This blade assembly is symmetrically constructed about its horizontal centerlines without camber.

The blade D-spar is of steel tubing, circular at the root where it is threaded to receive the attaching socket fitting, for mounting to the rotor head assembly.

The blade leading edge is a formed stainless-steel nose cap with a balance weight assembly bonded into it. The leading-edge assembly is bonded to the forward edge of the D-spar.

Twelve boxed fairings, consisting of fiberglass skins bonded to airfoil-shaped aluminum ribs, are bonded to the aft side of the D-spar. The trailing edge is formed by bonding a blade-long laminated stainless-steel strip into a special slot in the aft edge of the boxed fairings. Movable balance

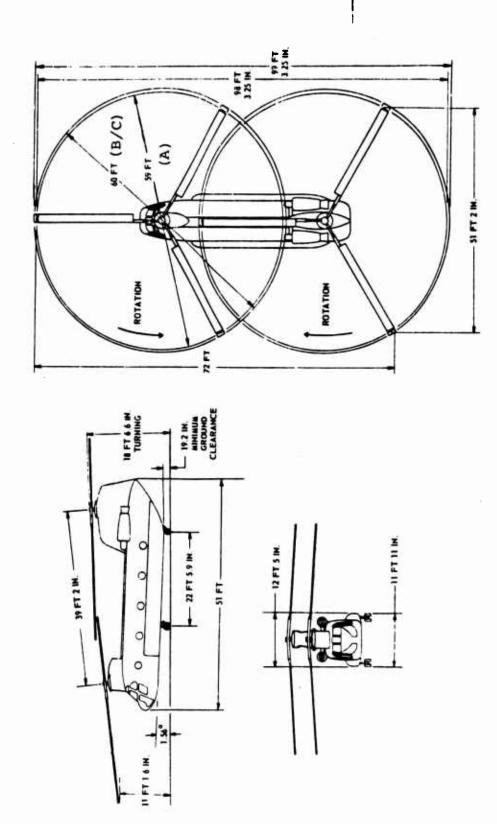


FIGURE 1. CH-47 HELICOPTER ROTOR SYSTEM.

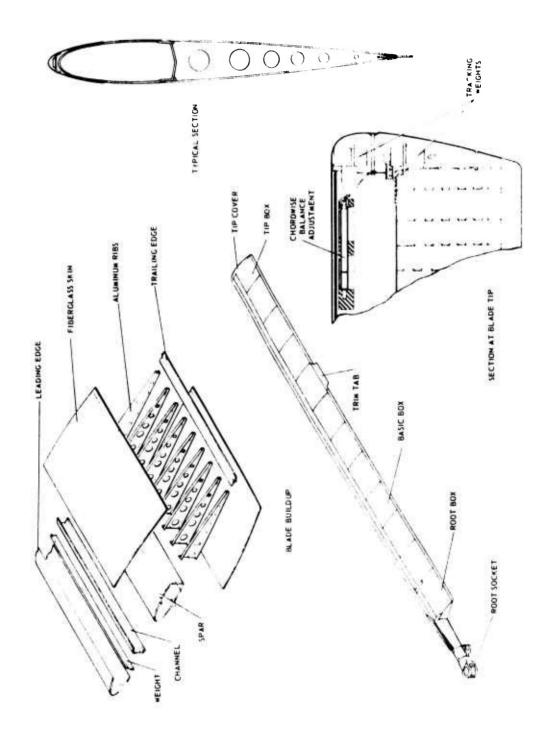


FIGURE 2. CH-47A ROTOR BLADE ASSEMBLY.

and tracking weights are installed on stainless-steel fittings riveted to the tip end of the D-spar. These weights are used to make balance and tracking corrections at the factory. A removable tip cover allows access to these weights. A blade tie-down fitting is located at the blade tip on the bottom surface.

### CH-47B/C Rotor Blades

The CH-47B/C rotor blade assembly as shown in Figure 3 is a nonsymmetrical cambered airfoil. The blade assembly consists of a D-spar, an attaching socket, a nose cap assembly, nine boxed fairings, a trailing-edge strip, tip balance provisions and a simplified tip cover. Construction of this blade is similar to the CH-47A blades except for the boxed fairings and nose cap as shown in Figure 3.

### DATA EXTRACTION PROCESS

A specific data extraction process was developed and applied to locate, extract, and describe CH-47 rotor blade discrepancies investigated for this report. This was done by the use of an alphanumeric coding system capable of identifying practically all important discrepancies occurring to any part of the entire structure of a CH-47 rotor blade. This alphanumeric system provided different codings for the CH-47A and CH-47B/C blades to allow for blade design differences.

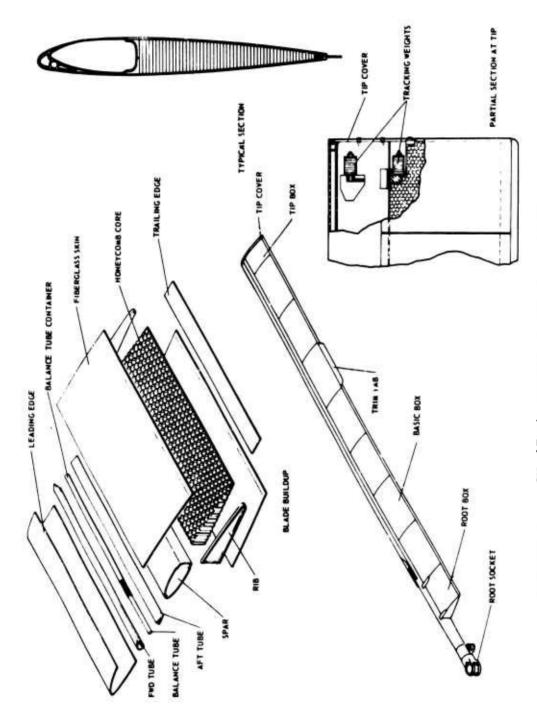


FIGURE 3. CH-47B/C ROTOR BLADE ASSEMBLY.

### BLADE REMOVALS ANALYSIS APPROACH

### Data Limitations and Use

The data included in this report were compiled from the existing Boeing-Vertol records which have been kept on rotor blades removed elsewhere and shipped to Boeing-Vertol for inspection, repair and scrappage.

The removal dates of interest to this blade removal study are shown in Table II. Note that the time period of interest varies among the CH-47A, B and C model helicopters.

The helicopter f'ight time accumulated up to the removal dates shown for the CH-47B and CH-47C models have been averaged to provide a consistent basis for the CH-47B/C analysis, as these have not been considered separately.

### Loss of Data Due to Unusual Incidents

No data limitations were imposed due to blade damages incurred from unusual field experiences. It could have been decided that blade removal data derived from blade overstress caused by in-air and massive nearby explosions, severe blade flapping due to extreme windstorms, or close helicopter over-flights should have been excluded. However, it was felt that the exclusion of these unusual experiences would provide a distorted view of the complete in-the-field experience; therefore, this data was included.

Examples of two unusual incidents which occurred in RVN and which subjected a large number of CH-47 helicopter blades to severe damage beyond their design limits were:

- 1. Typhoon Frieda, in November 1967
- 2. The Camp Evans ammunition dump explosion, in May 1968

Fifty CH-47 rotor blades were involved in the typhoon incident. Of these fifty blades, nine forward and nine aft blades were X-ray diffraction inspected at the depot and were accepted with return to service. Twelve forward and twelve aft blades were X-ray diffraction inspected at the depot, with subsequent rejection for scrappage. The remaining eight blades were severely damaged and were scrapped without further inspection.

AND	NG-VER	SING-VERTOL KEPAIK/OVERHA	BOEING-VERTOL REPAIR/OVERHAUL/SCRAPPAGE INSPECTION RECORDS - DATES	NSPECTION RECORDS	- DATES
				CORRESPONDING	
HELICOPTER LOC	ROTOR	BLADE PART NUMBER	REMOVAL DATES FOR BLADE INSPECTION	ACCUMULATED FLIGHT HOURS FOR DATES SHOWN	EQUIVALENT BLADE FLIGHT HOURS
CH-47A For	Forward	114R1002	July 1, 1962 thru March 1, 1971	650,206	1,950,618
Aft		114R1002	July 1, 1962 thru March 1, 1971	650,206	1,950,618
CH-47B FOI	Forward	114R1502	June 1967 thru November 1, 1970	159,419	478,257
Aft		114R1502	June 1967 thru October 8, 1970	157,914	473,742
CH-47C FOI	Forward	114R1502	April 1968 thru November 1, 1970	138,694	416,082
Aft		114R1502	April 1968 thru October 8, 1970	136,694	410,082
TOTALS:				1,873,133	5,679,399
Data Germé	does n	Data does not include aircraft Germany, Korea and Alaska, but	Data does not include aircraft flight time incurred in Germany, Korea and Alaska, but does include CONUS and	e incurred in de CONUS and RVN.	

The thirty-three CH-47A and sixty-one CH-47B rotor blades that were involved in the Camp Evans explosion were shipped to Boeing-Vertol for inspection and repair, as required.

### Blade Population Sizing

During this study, 5,488 blades were reviewed for removal experience. To keep the analysis results at a reasonable level of confidence, this blade population has not been diluted by a large number of categories. It did provide for the separation of all data into forward and aft rotor blade data.

It was felt that the different operational characteristics between these two locations may produce different effects in the externally-caused or inherent discrepancies of these blades. Since blade construction is the same for blades used at both locations, then blade design is eliminated as a possible factor of any differences that resulted from this study.

### Determination of Reasons for Removal

Reasons for blade removal, where blades are either repaired or scrapped, have been organized into three major groups based strictly on blade discrepancies. One group concerns inherent blade failures and discrepancies, the second concerns external causes of blade damage or failure, and the third concerns scheduled reasons for blade removal.

The first group essentially includes those discrepancies associated with inadequacy of blade design to withstand actual environmental conditions encountered during field operations. The second group concerns blade failure induced by external influences as foreign object damage, combat, and the like. Included in this group are those blade discrepancies caused by errors due to inadequate shop or field repairs, handling, shipping or maintenance. Also included in this group, for the purpose of records only, are those blades removed without adequate or valid removal reasons. The latter group includes those blades received at the depot and inspected with the result that no damages of the kind reported were found.

This study will be concerned with the unscheduled removal reasons as shown in Table III and the scheduled removal reasons as shown in Table IV.

The Boeing-Vertol repair evaluation reports investigated in the study followed the failure code given by TM-38-750, Reference (1).

It should be noted that where blade damage cause was unknown at the time of removal, this removal analysis included a close review of all recorded discrepancies for these blades to determine what discrepancy would have been the major reason for blade removal for repair.

Appendix II shows the detail and depth to which this removal analysis was conducted. In particular, Figures 29, 30 and 31, as well as the accompanying discussion within this appendix, are of interest.

TABLE III. ROTOR BLADE UNSCHEDULED REASONS FOR REMOVAL/SCRAPPAGE			
TYPE OF DISCREPANCY	REASON FOR REMOVAL/ SCRAPPAGE	DESCRIPTORS	
	Deterioration	Missing Bare Steel Eroded Rippled Water Migration	
Inherent Caused Discrepancy	Unbond	Bulged Blistered Bond Void	
	Excessive Vibration	Beyond Tolerance Vibration	
	Eroded	Eroded & Other Worn	
	Corrosion	Corroded & Other Peeling Chipped Stained Seized Water Migration Pitted	
	Delamination	Voided Grazed Cracked Split	
	Cracked	Creased Grazed Cracked & Other Split	
	Fretted	Worn Fretted	
	Imbalance	Tip Rod Loose Imbalance	
External Caused Discrepancy	Foreign Object Damage (F.O.D.)	Dented Broken Torn Punctured Scored Bent	
	Combat Damage	Broken Scored Dented Punctured Torn Spar/Socket Damage	

TABLE III - Continued						
TYPE OF DISCREPANCY	REASONS FOR REMOVAL/ SCRAPPAGE	DESCRIPTORS				
	Overstress	Overstress & Other Bent Collapse Torn Minor Damage				
	Crashes/Strikes	Bent Collapse Torn Minor Damage				
Error Caused Discrepancy	Manufacturing/Shipping Maintenance/Repair Shop Error and/Inadequate Field Repair	Human Error				
No Valid Removal	No Known or Valid Reason for Removal	No Known Removal Cause				
	Unknown/Misc.	Miscellaneous				

TABLE IV. ROTOR BLADE SCHEDULED REASONS FOR REMOVAL/SCRAPPAGE							
TYPE OF DISCREPANCY	REASON FOR REMOVAL/ SCRAPPAGE DESCRIPTORS						
Time Change	MWO Compliance No defect - Blade Removed for Scheduled Maintenance	MWO Sched. Maint.					
	Retired Blade EIR Engineering Evaluation	Retired EIR					
Other	No Defect - Blade Removed to Facilitate Maintenance of Other Component(s)	No Defect					
	Unknown/Misc.	Miscellaneous					

### CH-47A, B and C Blade Inspection Requirements

The CH-47 helicopter blade inspection requirements are discussed below. These requirements are noted herein to establish the criterion against which blades have been removed and scrapped.

Field inspection for serviceable CH-47A blades follows the minimum requirements noted in TM 55-1520-209-20-1, Reference (2), and for serviceable CH-47 B/C blades follows the minimum requirements noted in TM 55-1520-227-20-1, Reference (3). When a blade does not satisfy these conditions, it must be repaired or replaced, as applicable. For those blades sent back for depot rework and repair at the manufacturer's facility, the requirements of TM 55-1520-209-35-2 for the CH-47A blades, Reference (4), and of TM 55-1520-227-35-3 for the CH-47B and CH-47C blades, Reference (5), are followed. Partial or full teardown of 20% to 30% of the blades sent to the depot will occur. These teardowns will assure a complete determination of the extent of blade damage or deterioration.

### Blade Identification - Overhaul and Retirement Data

Blade identification by dash number, overhaul time (hours), and blade retirement time (hours) for CH-47A rotor blades are shown in Table V.

Blade identification by dash number, blade overhaul time, and blade retirement time in blade hours for CH-47 B/C rotor blades are shown in Table VI.

Data for Table V has been derived from TM 55-1520-209-20-1, Reference (6), and data for Table II from TM 55-1520-227-20-1, Reference (7).

TABLE V. CH-47A BLADE OVERHAUL AND RETIREMENT HOURS DATA

COMPONENT	PART NUMBER	RETIREMENT INTERVAL (BLADE HRS.)		
Forward Rotor Blades	114R1002-27	3600		
Aft Rotor Blades	114R1002-28 thru -78	2400		
	114R1002-80 thru -92	2400		

TABLE VI. CH-47B/C BLADE OVERHAUL AND RETIREMENT HOURS DATA

				INTERVAL	DEMI DEMINI
COMPONENT	PART NUMBER	CH-47B	(BLADE CH-47C T55-L-7C	HRS.) CH-47C T55-L-11	RETIREMENT INTERVAL (BLADE HRS.)
Forward Rotor Blades	114R1502-9 114R1502-13 114R1502-15 114R1502-17 114R1502-23 114R1502-25 114R1502-27 114R1502-29 114R1502-31 114R1502-33	3600 3600 3600 3600 0/C 3600 3600 3600 0/C	3600 3600 3600 3600 3600 0/C 3600 3600 0/C	* * * * * O/C * * O/C	6000 6000
Aft Rotor Blades	114R1502-10 114R1502-14 114R1502-16 114R1502-18 114R1502-24 114R1502-26 114R1502-28 114R1502-30 114R1502-32	1500 1500 1500 1500 1500 0/C 1500 1500 0/C	1500 1500 1500 1500 1500 0/C 1500 1500 0/C	* * * o/c * * o/c	    4000   4000

Not installed in helicopter noted
 O/C - On condition removal, see References (2) and (6)

### Reasons for Removal Versus Frequency by Blade Removal

It is of primary interest to determine the quantity of blades removed for various reasons. This determination will establish a firm basis for the subsequent calculation of blade means.

This determination took two forms: one, a tabulation of the discrepancies and quantities based upon the reasons for removal, and second, a graphical display of the same information for better understanding of the distributions found.

### Calculation of Means

In this study, the calculation of certain means representative of blade operating experience includes the determination of mean-time-between-removals, mean-time-to-removals, and mean-time-between-unscheduled removals. Since nearly all of the same blade removal data is used to derive these various means and their derivations are similar, the derivation of only two of these will be discussed in detail. It should be noted here that blades removed for repair and scrappage are both included.

### (1) Calculation of MTBR values.

The mean-time-between-removals (MTBR) for either the forward or aft rotor blades was calculated as three times the sum of all CH-47A or CH-47B/C helicopter operating flight hours accumulated over a selected time period divided by the total quantity of forward or aft blades removed for all causes over that time period of interest. Three times the sum of all helicopter flight hours is required as the CH-47 helicopter uses three-bladed rotors.

Thus, for the forward blades,

N

where N = Total quantity of helicopters involved

t; = Flight hours per helicopter

n = Total quantity of forward blades
 removed

Calculation of the MTBR for the aft blades was accomplished similarly.

### (2) Calculation of MTTR values

The mean-time-to-removal (MTTR) was calculated by obtaining each removed blade's operating time (in hours) accumulated up to blade removal and dividing by the quantity of forward or aft blades concerned.

Thus, for the forward blades,

$$\frac{\sum_{i=1}^{N} t_{i}}{n}$$

t<sub>i</sub> = Total time in blade flight hours
 per blade at removal

Calculation of the MTTR for the aft blades was accomplished similarly.

### (3) Calculation of MTBUR values

The calculation of mean-time-to-unscheduled removal (MTBUR) was accomplished similarly to the calculation for MTBR discussed above, except that blades removed for scheduled reasons were excluded from the sample of either forward or aft rotor blades.

### (4) Calculation of Means Example

To explain the derivation used to obtain the values shown in the subsequent means tabulations in this report, the following example is provided.

Per Table XI, page 34, the mean-time-between-removals of the forward rotor blade (MTBR $_{\rm F}$ ) for inherent discrepancies was derived as:

$$MTBR_{F} = \frac{3 (341 \times 1906 - 650, 206.7)}{682} = 2,860 \text{ Hr}$$

where 3 is the quantity of rotor blades on the forward rotor, 341 is the quantity of helicopters involved in the operational area and time period being considered (refer to Table II, page 10), 1,906.7 is the average flight time in hours per helicopter, 650,206 is the resultant helicopter flight time accumulated, and 682 is the quantity of forward blades removed for inherent discrepancies.

## <u>Determination of Discrepancy Locations Versus Types of Discrepancies</u>

This calculation was primarily concerned with the frequency of discrepancies or damages accumulated for particular blade samples and for various major areas and components of these blades. Both upper and lower surfaces of these blades were shown in the same chart. Forward and aft rotor blades were considered on separate charts. The discrepancy locations for blades that were scrapped for reasons found after removal have been discussed in the scrappage analysis section.

Results of this analysis were tabulated for the various areas as percentages of the total blade experience.

### BLADE SCRAPPAGE ANALYSIS APPROACH

### Data Limitation and Use

Data included in this portion of the report was derived from the same sources as that used for the blade removal study.

Primarily, the scrappage analyses differ from the removal analyses in that the reasons for scrappage are used as a basis for calculation.

The time period of interest is shown by Table II, page 10.

### Determination of Reasons for Scrappage

Reasons for blade scrappage, in general, have the same scope as those for removal as listed in Tables III, page 13, and IV, page 14.

### Calculation of Means

Only one set of estimated scrapped blade means is provided, since the scrapped blades are thoroughly investigated as a part of the removal analysis. This one set of means provided is that of mean-time-between-scrappage.

The calculation of the mean-time-between-scrappage (MTBS) applies only to those blades removed and eventually scrapped, whether the reason for scrappage was known beforehand or was determined after further blade inspection and/or blade teardown.

The calculation was accomplished similar to that for the MTBR as noted above, except that only scrapped blades were included for forward and aft rotors.

#### ANALYSES

#### CH-47 BLADE REMOVALS ANALYSES

The analyses presented herein follow the approaches discussed in the preceding section of the report. These analyses are grouped in chronological order of blade development and deployment:

- 1. CH-47A Forward and Aft Blades
- 2. CH-47B/C Forward and Aft Blades

Each group provides the following analyses:

- a. Major percentage of blade removals
- b. Frequency of blade removal vs. removal reasons
- c. Mean-Time-Between-Removal
- d. Mean-Time-To-Removal
- e. Mean-Time-Between-Unscheduled-Removal

Comparisons of the results of these analyses for forward and aft blades and the means are provided.

Table VII provides a review of the number of all blades that have been investigated for removals, repairs and scrappage. The actual accumulated flight time at removal of these blades and the equivalent time on the aircraft is given for comparison.

Note that the number of scrapped blades reviewed are included here for comparison.

TABLE VII.	NUMBER OF CH	1-47A AND	сн-47в/с віл	DES INVE	STIGATED FOR	REMOVALS	NUMBER OF CH-47A AND CH-47B/C BLADES INVESTIGATED FOR REMOVALS. REPAIRS AND SCRAPPAGE	SCRA PPAGE	
BLADES	S	УГТ	BLADES	ACCU TELLIT	ACCUPLIATED OF ON THE ON THE OWN THE O	ACCU TI SCRAP	ACCUMULATED TIME ON SCRAPPED BLADES	ACCUNULATED TIME ON AIRCRAFT	LATED IRCRAFT
HELICOPTER	BLADE LCCATION	QTY.	TIRE ON BLADES ! RETOVAL *	QTY.	TIME ON BLADES 3 PENOVAL •	QTY.	TIME ON BLADES 3 REMOVAL ●	HELICOPTEP FLIGHT TIME	EQUIVALENT BLADE FLIGHT TIME
CH-47A	Forward	2,126	1,028,473	1,932	945,627	194	82,846	650,206	1,950,618
	Aft	2,349	1,105,419	1,855	870,367	494	235,052	650,206	1,950,618
CH-47B/C	Forward	512	202,775	457	186,292	55	22,483	298,113	894,339
	Aft	501	185,067	430	159,758	7.1	25,309	294,608	883,824
TOTALS	Forward	2,638	1,231,248	2,389	1,125,917	249	105,329	948,319	2,844,957
	Aft	2,850	1.290.486	2,285	1,030.125	565	260,361	944,814	2,834,442
	A11 Blades	5,488	2,521,734	4,674	2,128,418	814	365,690	1,893,133	5,679,399

\* Time on blades at removal given in blade hours.

# CH-47A Forward and Aft Blades Removal Analysis

The removal status of 4,475 blades was reviewed; 2,126 of these were forward blades and 2,349 were aft blades.

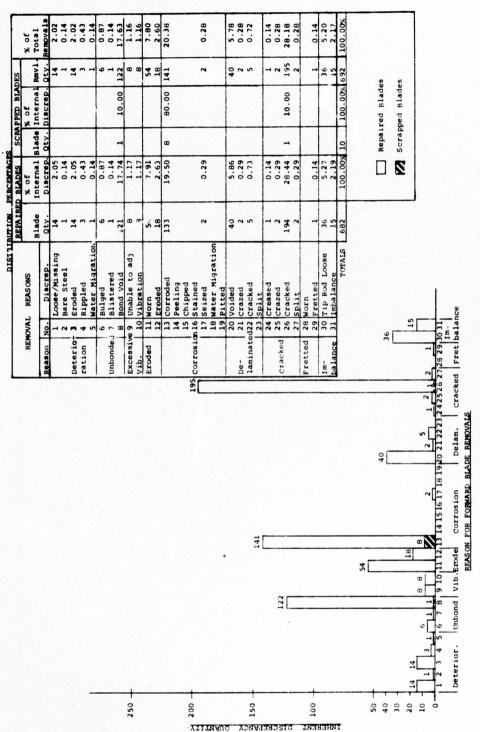
Table VIII summarizes the removal status for the most frequently occurring causes of removal for the forward blades. Table IX summarizes similar information for the aft blades.

Figures 4, 5 and 6 illustrate the quantity of forward blades removed for the reasons under study. Figures 7, 8 and 9 illustrate the quantity of aft blades removed for similar reasons. Note that scrapped blade quantities are identified. In these figures the reason for removal of a blade that is scrapped is used, not the reason for scrappage unless they coincide.

A summary of the percentages of CH-47A forward and aft blade removals versus reasons for removal is presented in Table X, page 32. For a comparison to percentages of CH-47B/C forward and aft blade removals, see Table XX on page 55.

ş		% OF TOTAL REMOVALS	2.54	•							1.88	6
47A	LADES	QTY.	440	20		2					40	
PERCENTAGES OF FORWARD BLADE REMOVALS - CH-47A	SCRAPPED BLADES	REMOVAL REASON	F.O.D Dented Overstressed Combat Demade -	Punctured Combat Damage -	Dented Crasher/Strikes (Winor						Remainder	equals 1,932 + 194 = 2,126.
SES OF FORW		8 OF TOTAL REMOVALS	15.52 12.98	9.13	5.69	3.76	3.29	2.73	2.54	1.88		90.87% removals
ERCENTA	ADES	QTY.	330 276	194	121	80	70	. SO	54 52	40 38	300	1,932* ard blade
TABLE VIII. P	REPAIRED BLA	REMOVAL REASON	F.O.D Dented Sched. Removal (Sched. Maint.)	Cracked Corrosion	Unbonded (Voids) F.O.D Punctures	Combat Damage - Punctures	Sched. Removal (Misc.) Overstressed	Sched. Removal	Eroded F.O.D Scored	Delaminated (Voided) F.O.D Bent	Remainder	TOTALS 1, * Total forward

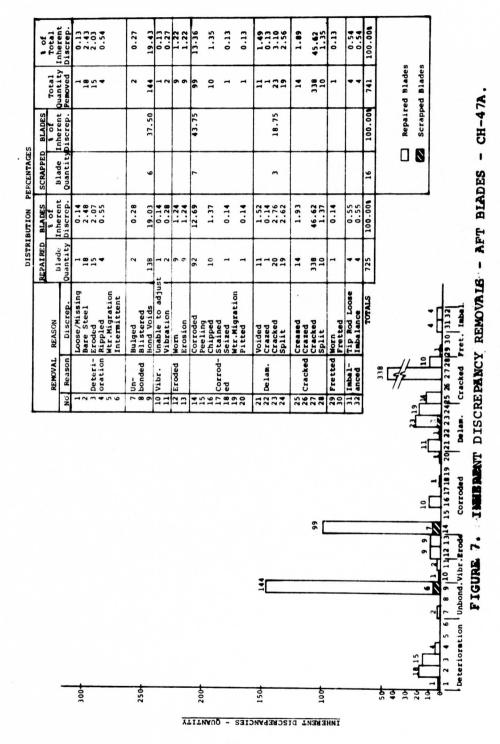
TABLE IX.	PERCENTAGES	OF	AFT BLADE REMOVALS - CH-47A		
REPAIRED BLAD	DES		SCRAPPED	BLADES	
REMOVAL REASON	QTY.	% OF TOTAL REMOVALS	REMOVAL REASON	QTY.	8 OF TOTAL REMOVALS
Sched. Removal (Maint.)	361	15.37	Overstressed	215	9.15
F.O.D Dented	250			. æ	1.62
Unbonded (Voids)	138	5.87	Combat Damage -	31	1.32
Corrosion	92	3.92	Punctures		,
Combat Damage	69	2.85	Sched. Removal (Retired Blades)	97	11.1
Overstress	64	2.72	F.O.D Punctured	15	0.64
Sched. Removal (Misc.)	09	2.55		15	0.64
F.O.D Scored	46	1.96			
	30	1.28			
Ö					
F.O.D Torn	59	1.24			
id	26 י	1.11			
F.O.D Bent	24	1.02			
Remainder	245	10.43	Remainder	61	2.59
TOTALS	1,855	78.978		494	21.038
TOCAL AIC DIAGE	ade removals	vais equais	1,855 + 494 = 2,349.		

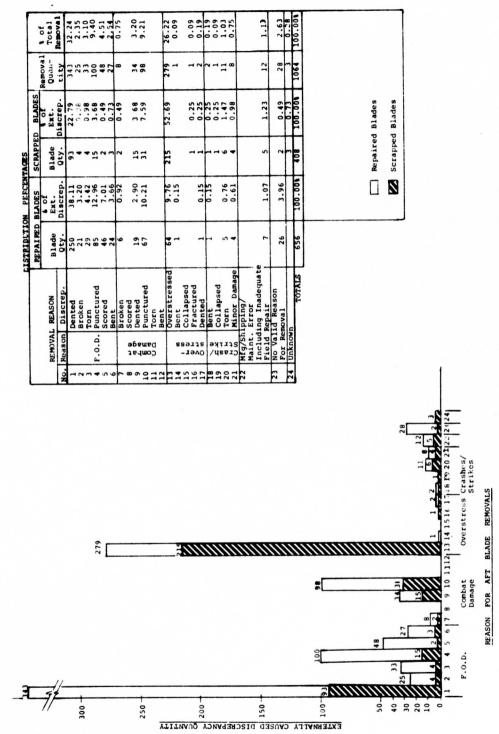


- FORWARD BLADES - CH-47A. INHERENT DISCREPANCY REMOVALS FIGURE 4.

Page	Second   19   19   19   19   19   19   19   1	A S	REMOVAL R		KEPAIK	ED BLADES	SCRAPP	REPAIRED BLADES SCRAPPED BLADES		
10   10   10   10   10   10   10   10	10   1   1   1   1   1   1   1   1   1	- Ree		EASON	Blade	% of External	Blade	% of External	Rmv1.	* of Total
10   10   10   10   10   10   10   10	10   10   10   10   10   10   10   10	P.(		Discrep.	Qty.	Discrep.	Otv.	Discrep.	Qty.	Removal
14   15   17   18   19   19   19   19   19   19   19	14   15   15   15   15   15   15   15	P.(	1	Dented	330	40.64	54	2	384	38.75
15   15   15   15   15   15   15   15	10	F.0	_	Broken	4	1.72			14	1.41
10   10   10   10   10   10   10   10	1   1   1   1   1   1   1   1   1   1		-	Torn	35	4.31			32	3.53
Secored   Seco	Secored   Seco		4	Punctured	119	14.65		2.23	123	12.41
Stricken   26   34.0   4   4   5   5   5   5   5   5   5   5	10   10   10   10   10   10   10   10		2	Scored	25	6.40		11:1	4,	6.60
10   10   10   10   10   10   10   10	10   10   10   10   10   10   10   10		9	Bent	38	4.67	-		98	3.83
Second   S	10   1   1   1   1   1   1   1   1   1		7	Broken	4	0.49			4	0.40
10   10   10   10   10   10   10   10	10   10   11   12   13   14   15   16   17   17   18   18   18   18   18   18			Scored	:			:	;	
10   10   10   10   10   10   10   10	10   10   10   10   10   10   10   10	CO		Dented	14	1.72	70	11.17		20.00
1   Spar/Socket   1   0.12   1   0.55   2     1   Spar/Socket   1   0.12   1   0.55   1     1   Spar/Socket   1   0.12   1   0.55   1   0.55   1     1   Spar/Socket   1   0.12   1   0.55   1   0.55   1     1   Spar/Socket   1   0.12   1   0.55   1   0.55   1     1   Spar/Socket   1   0.12   1   0.55   1   0.55   1   0.55   1     1   Spar/Socket   1   0.12   1   0.55   1   0.55   1   0.55   1   0.55   1     1   Spar/Socket   1   0.12   1   0.12   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0.55   1   0	1   2007   1   2017   1   2018   2   2   2   2   2   2   2   2   2	Dar		Punctured	80	3.85	97	14.52	901	10.70
10   10   10   10   10   10   10   10	1   2   2   2   2   2   2   2   2   2		=	Torn	_	:			,	
10   10   10   10   10   10   10   10	10   10   10   10   10   10   10   10		12	Spar/Socke	1	0.12	1	66.0	1	0.40
10   10   10   10   10   10   10   10	10   10   10   10   10   10   10   10		13	Overstress		8.25	44	24.58	111	11.20
10   10   10   10   10   10   10   10	10   10   10   10   10   10   10   10	00		Bent	_					
1   1   1   1   1   1   1   1   1   1	10   10   10   10   10   10   10   10	st	_	collapsed						
100   11   1   1   1   1   1   1   1	10   10   10   10   10   10   10   10		16	Fractured	1	0.12			-	0.10
10   10   10   10   10   10   10   10	105   1   105   105		17	Dented	1	0.12			-	0.10
Strikes   19 Collapse   19 C	100   11   11   12   12   13   14   15   15   15   15   15   15   15		18	Bent			_	0.55	-	0.10
3   1   0   0   0   0   0   0   0   0   0	Strikes   20   Torn   10   10   10   10   10   10   10   1	Cra		collapse			œ	4.46	œ	0.81
106   111   11   11   11   11   11   1	10   11   1   1   1   1   1   1   1	Str	_	Torn			1	0.55	-	0.10
10   11   1   1   1   1   1   1   1	106   111			Minor Dama		1.84		5.58	25	2.52
100   111	106   117   12   12   13   14   15   17   15   17   15   17   17   17	EL		Error .		3.20		3.91	33	3.33
105 106 111 107 112 113 114 115 115 115 117 115 117 117 117 117 117	105   110	Not	t Valid 23	No Valid R		1.84			15	1.51
100 000, 179   100 000, 199   100 00, 199   100 00,	100.00%   179   100.00%   191   100.00%   191   100.00%   191   100.00%   191   100.00%   191   100.00%   191   100.00%   191   100.00%   191   100.00%   191	Z	isc. 24				-	0.55	-	0.10
106   116   117	106   117		I			_	_	100 001	100	100
24 44 33 33 25 26 26 27 3 3 44 3 33 33 33 34 34 34 34 34 34 34	24 33 34 8 44 25			101		-	-	200.004	122	
33 20 20 20 33 25 4 10 11 25 6 7 8 10 10 11 11 11 11 11 11 11 11	33 20 20 20 20 20 20 20 20 20 20 20 20 20						]			
33	24 4 20 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1						][		Blade	
13   14   44   33   34   44   44   33   4   10   11   10   11   10   11   10   11   10   11   10   11   10   11   10   11   10   11   10   11   10	14						Z		Blade	
10   10   10   10   10   10   10   10	14   25   26   25   25   25   25   25   25							dling Error	/Ship	/buing/ uding
25 1 1 1 8 10 7 15 15 15 15 15 15 15 15 15 15 15 15 15	25 4 10 112 13 14 15 16 17 18 19 20 21 22 23 24 15 5 6   7 8 9 10 1112 13 14 15 16 17 18 19 20 21 22 23 24 Combat Damage   Overstress   Crashes / Strikes   Strikes	33					Tug	nednate Li	010	i i i
1 5 6 7 8 9 10 1112,1314 1516 1748 1920 212223   Combat Damage   Overstress   Crashes / Strikes   Strikes		25 10 7								
Combat Damage Overstress REASONS FOR FORMARD BLADE F	Combat Damage   Overstress   Crashes/  Strikes   Strik	21,22,23								
FOR FORWARD BLADE R	FOR FORMARD BLADE REMOVAL	es/								
		se 1								
	FIGURE S. FYTERNAL DISCREPANCY REMOVALS - FORWARD BLADES	20.21/22/23/24 es.	SOM BEACH		S S S S S S S S S S S S S S S S S S S	6	i i		į	KL P - HO - S

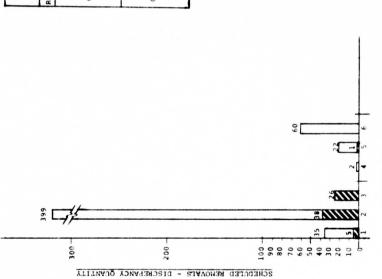
				REPAIRED	BLADES	SCRAPPED	ED BLADES		
		REMO	REMOVAL REASON		Jo 1		jo 1		jo 1
	Feason	No	Discrepancy	Blade Qty.	Sched. Removals	Blade Qty.	Sched. Removals	Removal Quantity	100
		7	MMO Compliance	32	7.24		1	32	7.22
	Time	~	No Defect (Sched. Maint.)	276	62.45	1	1	276	62.31
		~	Retired Blades	1	0.90	•	80.00	•	0.00
		1	EIR Engr.	2	0.45	:	:	2	0.45
	Š	0	Evaluation No Defect (to facilitate maint)	88	13.12	1	1	88	13.09
		9	Miscellaneous	70	15.84	1	20.00	11	16.03
		1	.vorals	4.38	100.00	5	100.00%	<b>F</b>	100.001
								Repaired Blades	ades
								Scrapped Blades	ades
ដ[									
<b>"</b>									
4 - 4   11	1								
Time Cng. Other									
SCHEDULED REMOVAL REASON									
FIGURE 6. S	SCHEDITLED REMOVALS	ZEN	OTATE - PC	DEM DI	ALL TO DETRIES OF ATTACH	Ç	AC 1 178		





EXTERNAL DISCREPANCY REMOVALS - AFT BLADES - CH-47A φ. FIGURE

				REPAIRED	D BLADES	SCRAPPED	D BLADES		
	EM	REMOVAL	REASON		f of		y of	Total	l of
Reason	No.		Discrepancy	Blade Oty.	Scheduled Removals	Blade Qty.	Scheduled Removals	Oty. Removed	Total Removals
	-		MMO Compliances	30	6.33	5	7.14	35	6.42
Time Change	7		No Defect (Sched- uled Maintenance)	361	76.16	38	54.29	399	73.35
	~		Retired Blades	1	1	56	37.14	36	4.78
	4		EIR Engineering	2	0.42	1	:	2	0.38
Other	2		No Defect (to facilitate maint.	21	4.43	٦	1.43	22	4.04
	9		Miscellaneous	60	12.66	-	ı	09	11.03
			TOTALS	474	100.001	70	100.004	544	100.00
							Repa	Repaired Blades Scrapped Blades	d e de ss



SCHEDULED REMOVALS - AFT BLADES - CH-47A

FIGURE 9.

TABI	TABLE X.	SUMMARY FORW	OF ARD	PERCENTAGES AND AFT ROT	ENTAGE: AFT RO	OF OR B	REMOVALS BLADES	1	СН-47А		9	
MAJOR		FORWARI	ROTOR	OR BLADE	DES *		Ì	AFT	ROTOR	BIA	+ 5:	
DISCREPANCY	Total Bla		Ref Bla	-H W	Scr Bla	Scrapped Blades	Total Blade	- All	Repaire Blades	ש	Scrapped Blades	apped
REMOVAL REASON	Qty.	Pct.	Qty.	Pct.	Qty.	Pct.	Qty.	Pct.	Qty.	Pct.	Qty.	Pct.
Deterioration	33	.5			1	0	38	1.62	38	9		0
Unbonded	129	6.07	128	6.02	7	0.05	146	•	140	5.60	9	0.26
Vibration	16	.7	16		1	0	m		3	۲.	t I	0
Erosion	72	۳.		۳.	!	0	18	0.77	18	0.77	!	0
Corrosion	143	.7		۳.	œ	0.38		.7		4.	7	0.30
Delaminated	47	•		. 2	1	0		2.30	51	2.17	m	0.13
Cracked	200		199		7	0.05	362	4.	362	15.41	1	0
Fretted	7	0.		•	1	0	-	0		0	1	0
Imbalance	51	2.4	S	4.	-	0	ω	3	8	3	1	0
F.O.D.	648	4.		• 6	09	œ.	7	.5	455	m.	121	5.15
Combat Damage	146	ω.		9	47	φ.		6		6		0
Overstress	113	5.31			44	2.07	œ		99	2.81		.2
Crashes/Strikes	35	9.		.7	20	6.		6		4	-	5
Error	33				7	۳.		.5	7	•	2	.2
No Valid Reason	15		15	0.70	1	0	28	1.19	26	1.10	7	
Miscellaneous	-	0		0	_	0.05	3	.1	1	0	m	
Time Change	312	14.67		14.48	4	0.19	460	5	391		69	6
Other	131	6.16	130	6.11	7	0.	84		83	3.53	٦	0
TOTAL	2126	100.00		28.06	194	9.13	2349	100.00	1855	6	494	21.04
									l			
* Percentages	ba	sed	ď	Н,	£ 2,	126 fc	3 .	blades	•			
r reicentages	ğ	sea upon	ש	total c	7	4	t blades	des.				

### CH-47A Forward and Aft Blades Means Analyses

A series of evaluations of the CH-47A rotor blades for their average removal characteristics based upon frequency of blade removal was accomplished. These calculations of the various removal means followed the approach outlined on pages 20 and 21. Results are given in blade hours.

Tables XI, XII, and XIII list the means determined for the major discrepant reasons for removal of CH-47A forward rotor blades.

Tables XIV, XV, and XVI list similar determinations accomplished for the CH-47A aft rotor blades.

Table XVII presents a summary of the results of these analyses for both CH-47A forward and aft blades.

		RETURNED J	JAPES	SCPA	SCPAPPED BLADES	S	TO	TOTAL BLADES	5
		Total			Total			Tot	1
	otv. of	Fwd. Bld.	MTBP	otv. of	Fyd. Bld.	MTBR	04 0	Fyd. Bld.	MTIB
REASONS FOR REMOVAL	Blades	Flight			Flight			Flight	
	Removed.	Hours		Penoved	Hours		Removed	Hours	
Inherent Discrep.	Z89		2,860	10		195,062	692		2,819
Deterioration	33		59,109				33	-	59,109
Cuponded	128		15,239	7		1,950,618	129		15,121
Excessive Vibration	16	-	121,914				16	_	121,914
Erosion/Wear	7.5	1,950,618	27,092		1,950,618		72	1,950,618	27,032
Corroded	135		14,449	œ	-	243,827	143	-	13,641
Delamination	47		41,503				47		41,503
Cracked	199		9,802	-		1,950,618	200		9,733
Fretted	-		1,950,618				-		1,950,618
Imbalance	51		38,247				51		38,247
Externally-Caused Discrey.	771		2,530	171	•	11.407	942	-	2,071
Combat Damage	66	1.950,618	19.703	47	1.950.618	41.503	770	1 950 618	13.260
Overstressed	69		28,270	4.	-	44.332	113	-	17.762
Crasnes/Strikes	15	-	136,041	2.0	•	97,531	35	•	55,733
No Valid Removal Reason	15	1,950,618	130,041	L	1,950,618	1,950,618	16	1,950,618	121,914
Lrror	26	1,950,618	75,024		1,950,618	278,660	33	1,950,618	59,109
Scheduled Removal	438		4,453	5		390,124	443	-	4.403
Time Change	308	1,950,618	6.332	7	1.950,618	487,654	312	1,950,618	6.152
Other	130		15,005			1,950,618	131		14.890
All Causes	1,932	1,950,618	1,009	194	1,950,618	10,055	2.126	1,950,618	917

	REPAIRED	THED BLADES	S	SCI	SCRAPPED BLADES	ES	TOTAL	AL BLADES	
		13			ᆫ			Total	
	Qty. of	Fwd Blade	MTTPE	Oty. of	Fwd Blade	MTTR		Fwd Blade	MITTR
REASONS FOR REMOVAL	Blades	Flight	•	Blades	Flight		_	Flight	
	Removed	Hours		Removed	Hours	***	Removed	HOUL	1
Inherent Discrepancies	682	320,803	470	21	5,476	248	36	15,427	191
Chonded	128	59,167	462	7	24	24	129	59,191	459
Excessive Vibration	16	7,267	454				16	7,267	454
Erosion/Wear	72	35,839	498				72	35,839	864
Corrosion	135	64,209	476	<b>o</b> o	5,114	6 39	143	24,923	683
Delamination	47	24,948	531	•	ć	000	400	24,948	231
Cracked	199	91,863	462	-	338	3.38	200	107'76	100
Fretted	7.5	99	431				7 5	21.984	431
Imbalance	10.	247 103	100	171	60 51B	35.4	942	407.621	433
Externally Caused Discrepancies	1/1	570 767	450	109	23.572	100	8	294.339	151
Combat Damage	66	40.775	412	47	14,607	311	146	55,382	379
Overstressed	69	30,250	438	44	17,780	404	113	46,030	425
Crashes/Strikes	15	5,311	354	20	4,559	228	35	9,870	282
No Valid Reason for Removal	15	4,011	797	-	267	267	16	4,278	267
Error A	25	7,748	862	7	1,596	228	33	9,344	283
Scheduled Removals	438	265.962	809	ıΩΙ	14,989	2,998	1	280,951	634
MWO Compliance	32	16,894	875				350	176 650	270
Scheduled Maintenance *	276	176,659	049				017	26 524	457
To Facilitate Maintenance	20 0	120,02	100				2	1.484	742
EIK	•	101.11		4	13.429	3,357	4	13,429	3,357
Miscellances	70	44,401	634	-	1,560	1,560	7.1	45,961	647
AII Causes	1,932	915,627	490	194	82,846	427	2,126	1,028,473	484
No Defect									
△ Manufacturing/Shipping/Handling Error Including Inadequate Field Rejair	g/Handling	Errer Incl	uding Inac	decuate Fi	eld Regair				

	REP	REPAIRED BLADES	5.	SCRAPPED	PED BLADES	ES	F	TOTAL BLADES	8
		ta			ota	•		Total	
	Oty. of	Fwd. bld.	"TBUR	ity. of	Fwd. Bld.	MTBUP	Qty. of	Fwd. Bld.	MTBURE
REASONS FOR REMOVAL	Blades	Flight		Blades	Flight		Blades	Flight	
	Removed	Hours		Removed	Hours		Removed	Hours	
Inserent Disersp.	682	-	2,860	21	-	195,062	11	1	59,109
Unbonded	128		15.239	_		1,950,618	129		15,121
Excessive Vibration	16	_	121,914				16		121,914
Erosion/Wear	72	1,950,618	27,092		1,950,618		72	1,950,618	27,092
Corroded	135	_	14,449	80	_	243,827	143	_	13,641
Delamination	47		41,503				47		41,503
Cracked	195		9,802	-		1,950,618	230		950,619
Imbalance	51	-	38,247		-		51	-	38,247
Externally-Caused Discrep.	177		2,530	171		11,407	942	-	2,071
Foreign Object Damage	288	<b>-</b>	3,317	09	-		648	_	3,610
Combat Damage	66	1,950,618	19,703	47	1,950,618		146	1,950,618	13,360
Overstressed	69	-•	28,270	44	-	44,332	113	-•	17,262
S.	15		130,041	20		_	35		25, 732
No Valid Removal Reason	15	1,950,618	130,041	-	1,950,618	-	16	1,950,618	121,914
Error •	97	1,950,618	75,024	,	1,950,618	7	33	1,950,618	59,109
All Causes	1,494	11,950,618	1,306	189	1,950,618	10,320	1,683	1,950,618	1,159

	REI	REPAIRED BLADES	S3	SC	SCRAPPED BLADE	ES	-	TOTAL BLADES	
		Total						Total	
REASONS FOR REMOVAL	Oty. of	Aft Blade	MTBR	Qty. of	Aft Blade	MTBP	Oty. of	Aft Blade	MTBR.
	Blades	Flight	<	Blades	Flight	<	_	Flight	<
	Removed	Hours		Removed	Hours		Removed	Hours	
Inherent Discrepancies	725	-	2,690	16	-	121,914	7		7,637
Harris and Arion	9 9		34,334	,			9	_	51,332
Freedown Unbration	0.		13,933	٥		325,103	146		13,360
Stocker Many	7 0	9 6 7 0 7 9 1	100,200		012 030		2 0		907,000
Corrosion	104	610.000.1	18.755	,	BTO'NCK T	278.659		B19'006'1	108,367
Delamination	51		38,247	•			51		38.247
Cracked	362		5,388	٣	-	650,236	365		5,344
Pretted		_	1,950,618				~		2.950.618
Impalance	8	•	243,827		~			_	243,827
Externally Caused Discrepancies	623	_	3,131	398		4,900	1,021		1,910
Foreign Object Damage	453		4,287	151		16,121	576		3,386
Combat Damage	92	1,950,618	21,202	48	1,950,618	40,638	140	1,950,618	13,933
Overstressed	99	_	29,555	217		8,989	283	_	6,893
	10		195,062	12	-	162,552	22		88,664
No Valid Reason for Removal	26	9	75,024	5	1,950,618	390,124	31	1,950,618	62, 923
Error	7	1,950,618	278,680	5	1,950,618	390,124	21	1,950,618	162,552
Scheduled Removals	474	-	4,115	70		27,866	544		3,586
MANO COMPLIANCE	٠ ٢		65,000	٠. د		390,124	35	_	55,732
Scheduled Faintenance	105	_ ;	2,403	<b>30</b> ,		51, 332	399		4,889
raciticate maintenance	7 .	010,000,1	000,350	-	1,950,618	# T9 '006'T	77	1,950,618	999,88
701100	•		2121303	3.6	-	75 034	7 /		975,309
Miscellaneous	09	-	32.510	•	-	70'7'	1 4	•	12,026
ATTANSOR	2 20	1 650 616	4 8 5	101	ľ	0.50		-	7
- 11	1,622	-11	1,052	434	819,056,1	3,950	2,349	1,950,618	836
<ul> <li>Manufacturing/Shipping/Handling Error Including Inadequate Field Repair</li> </ul>	dling Erro	r Including 1	Inadequate	Field Rep	air.				

Total Aft Bld. Flight Hours 447,756 23,168 81,741 1,851 4,870 356,112 201,665 47,927 99,256 10,436 72,064 33,958 219,466 7,264 12,417 4,805 284,329 9,903 179,703 37,626 Oty. of Blades Removed 741 741 146 1,021 576 140 283 22 22 31 12 13 135 399 18 111 51 365 2,349 MTTRA 364 366 355 364 365 365 365 111 1,144 497 298 488 284 2,285 BLADES Total Aft Bld. Flight 44,321 17,041 79,069 4,385 2,557 2,057 1,492 18,885 294 Hours 5,550 59,401 1,703 2,382 1,465 SCRAPPED Oty. of Blades Removed \* Manufacturing/Shipping/Handling Error Including Inadequate Field Repair. 9 26 ~ MTTRA 2431 445 445 327 272 460 MEAN-TIME-TO-REMOVAL - AFT BLADES - CH-47A Total Aft Bld. Flight Hours REPAIRED BLADE 442,206 23,168 80,038 1,851 10,436 69,682 33,958 218,001 211,296 1157,344 1157,344 20,187 2,879 2,879 2,748 2,748 2,748 2,748 2,748 2,748 6,859 27,626 Oty. of Blades Removed 455 455 10 26 26 3 104 51 362 Externally-Caused Discrepancies Foreign Object Damage REASONS FOR REMOVAL Facilitate Maintenance Crashes/Strikes
No Valid Removal Reason MWO Compliance Scheduled Maintenance Excessive Vibration Erosion/Wear Retired Blades TOTAL All Causes eduled Removals Inherent Discrep. Deterioration Combat Damage EIR Miscellaneous Delamination Overstressed Corrosion Imbalance TABLE XV. Unbonded Cracked Fretted

	REPAIPED			SCR	SCRAPPED BLADES	83	TATOT	AT BIADEC	
		Total			C		101	1	
REASONS FOR REMOVAL	otv. of	Aft Blade	MTBIID	30	. C. S.			Total	
	Blades	Flight	A	Plader	Art Blade	MTBUR	Oty. of	Aft Blade	MTBUR
	Removed	Hours		brades	Fiignt		Blades	Flight	
Inherent Discrepancies	775		200	Removed	Hours		Removed	Hours	
Deterioration	ila.	•	2,096	41		121,914	741		
Unbonded	240		17,532				38		
Excessive Vibration	7.		13,933	9		325,103	146		
Erosion/Wear			907,000				3		9
Corroded	104	1 950 619	100,300	•	_	_	18		108,367
Delamination		010 00001	38.247	,	1,950,418	278,659	111	1,950,618	17,573
Cracked	362		5,388	,		200	51	-	
Fretted	-		1 050 610	,		907'069	365		
Imbalance	80		243.827				(		1,950,618
Externally-Caused Discrepancies	623		1.13	198		A GAN	200		243,827
Foreign Object Damage	455		4.287	121		4,300	1.021		
Combat Damage	9.5	1,950,618	21.202	48	1 950 619	171.0	9/0	-	
Overstressed	99		29.555	217	010'00'	0000	140	1,950,618	
	10		-	12		162 653	583		6,833
No Valid Removal Reason	26	1,950,618		3	1.950.618	140, 173	777	100	
	7	1,950,618	2	5	1,950,618	1	151	1 950,010	62,923
All Causes	1,381	1,950,618	1,412	424	1,950,618	_	1.805	1 950 619	1

					EXTERNALLY	ERROR		NO VALID
	FLADE		COMBINED	INHERENT	CAUSED	CAUSED	SCHEDULED	REMOVAL
			VALUES	DISCREPANCY	DISCREPANCY	DISCREPANCY	REMOVALS	REASON
		Repaired	1.009	2.860	2,530	75.624	4.453	130,041
	MTBR	Scrapped	10,055	195,062	11,407	278,660	390,124	1,950,618
		Total	917	2,819	2,071	59,109	4.403	121.914
POMMARD		Repa: red	190	470	450	298	809	267
_	HTTR	Scrapped	427	248	354	228	2.997	267
BLADES		Total	184	472	433	283	634	267
-		Repaired	1,306	2.860	2,530	75,024	Y. Y.	130,041
	MTBURF	Scrapped	10,320	195,062	11,407	278,660	.A. N.	1,950,618
	-	Total	1,159	2,819	2,071	59,109	. A. A.	121,914
-		Repaired	1,052	2.690	3,131	278.659	4,115	75,024
	MTBRA	Scrapped	3.950	121,914	4.900	390,135	27,866	390,124
		Total	830	2,632	1.910	162,552	3,586	62,923
AFT		Peraired	694	610	339	393	431	379
	A I IE	scrapped	476	347	364	1	1,144	511
BLADES	1	Total	471	<b>\$09</b>	349	004	523	101
		Repaired	1.412	2,690	3.131	278,659	V.A.	75,024
	MIBCKA.	scrapped	009.	121,914	4.900	390,124	٠.٨.	390,124
1		rotal	1,080	2,632	1,910	162,552	N.A.	62,923

# Discrepancy Locations Versus Types of Discrepancies

Data included herein has been based upon 'Reasons for Removal' only.

This investigation simplified the amount of data handled by confining the results to discrepancy locations versus types of inherent discrepancies and to externally-caused discrepancies only.

Figures 10 and 11 illustrate the results obtained for the CH-47A forward blades. Figures 12 and 13 illustrate similar results obtained for the CH-47A aft blades.

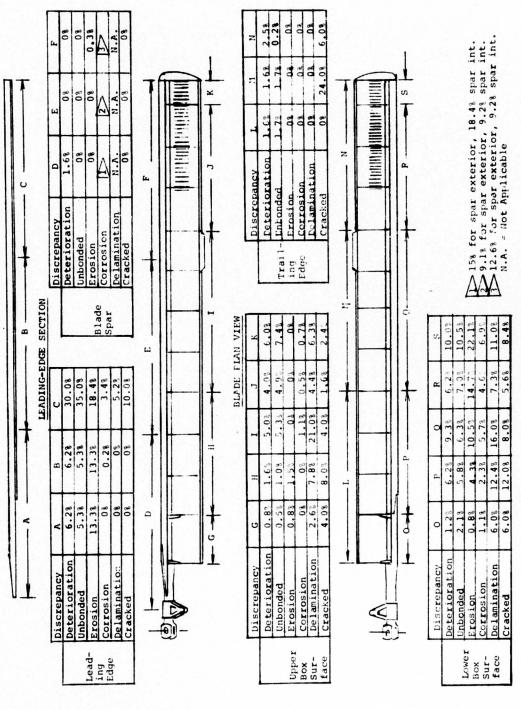
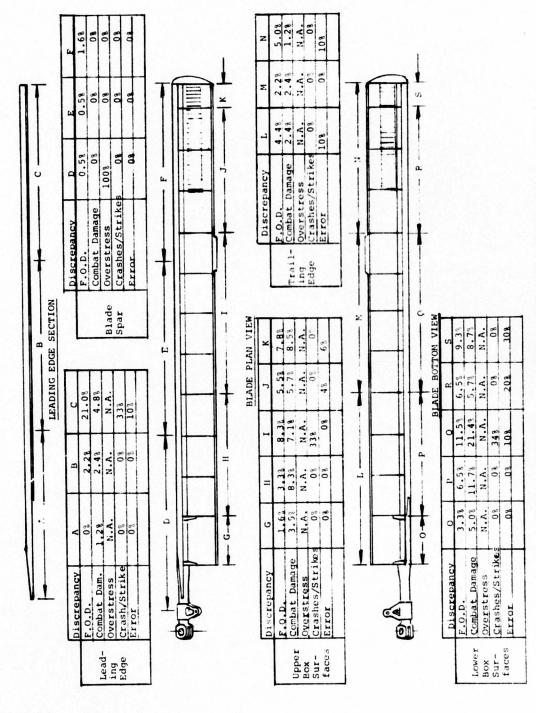


FIGURE 10. INHERENT DISCREPANCY LOCATIONS - FORWARD BLADES - CH-47A.



EXTERNAL DISCREPANCY LOCATIONS - FORWARD BLADES - CH-47A. FIGURE 11.

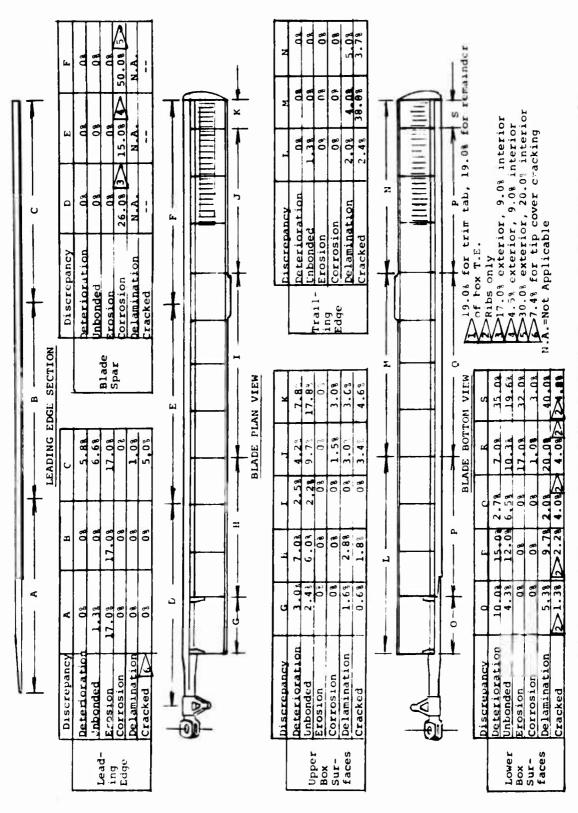
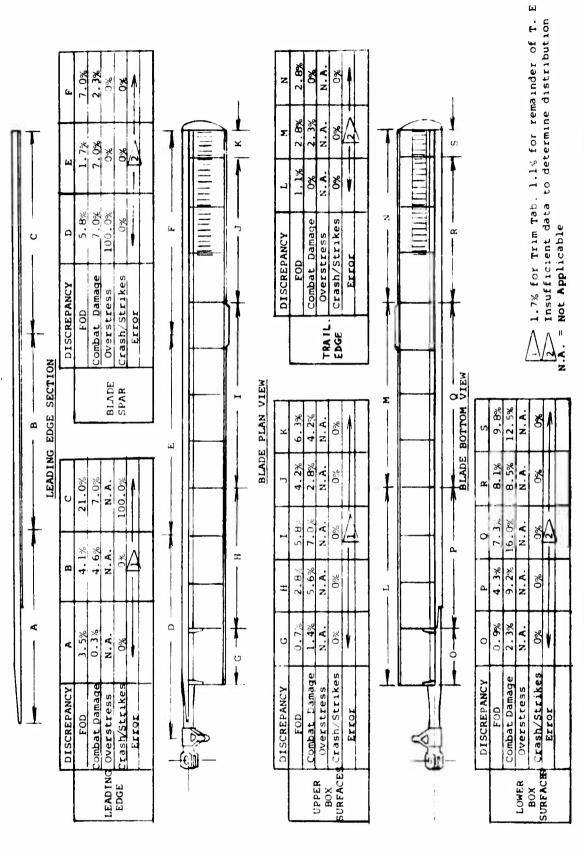


FIGURE 12. INHERENT DISCREPANCY LOCATIONS - AFT BLADES - CH-47A.



- AFT BLADES - CH-47A. FIGURE 13. EXTERNAL DISCREPANCY LOCATIONS

### CH-47B/C Forward and Aft Blades Removal Analysis

The removal status of 1,013 rotor blades was reviewed, 512 of which were forward blades and 501 were aft blades.

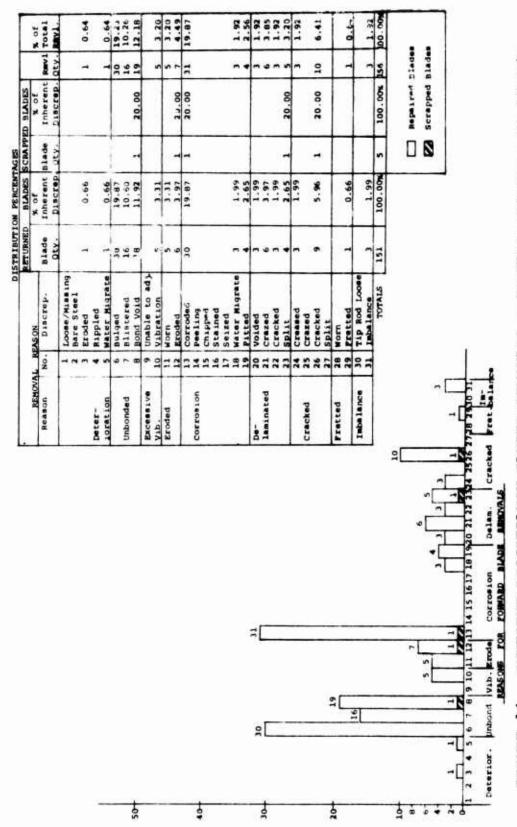
Table XVIII summarizes the removal status for the most frequently occurring causes of removal of the forward blades. Table XIX summarizes similar information for the aft blades.

Figures 14, 15 and 16 illustrate the quantity of forward blades removed for the reasons under study. Figures 17, 18, and 19 illustrate the quantity of aft blades removed for similar reasons. Note that scrapped blade quantities are identified. In these figures the reason for removal of a blade that is scrapped is used, not the reason for scrappage unless they coincide.

A summary of the percentages of CH-47B/C forward and aft blade removals versus reasons for removal is presented in Table XX, on page 55; for a comparison to the percentages of CH-47A forward and aft blade removals, see Table X, page 32.

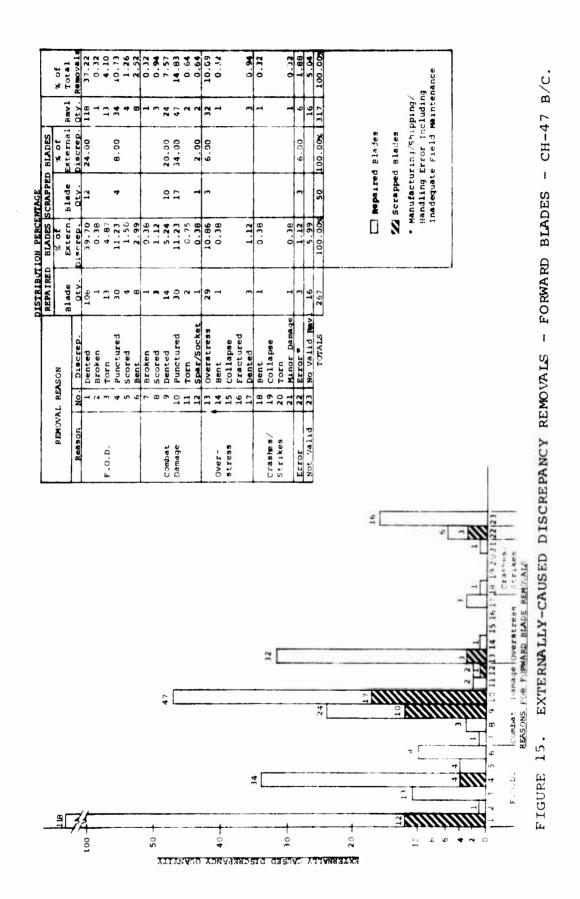
TABLE XVIII, P	ERCENT	AGES OF FORW	PERCENTAGES OF FORWARD BLADE REMOVALS - CH-47B/C	47B/C	
REPAIRED BL	BLADES		SCRAPPED BLADES	ADES	
REMOVAL REASON	QTY.	% OF TOTAL REMOVALS *	REMOVAL REASON	QTY.	% OF TOTAL REMOVALS ★
F.O.D. Denting F.O.D. Punctures Combat Damage Punct. Unbond.(Bulged) Boxes Corrosion Overstress No Defect-Sched.Maint. Box - Bond Voids Unbonded - Blistered No Valid Rem. Reason Combat Damage - Dent F.O.D. Torn No Defect - To Facilitate Maint. Remainder	106 30 30 30 30 23 18 16 16 10 457	20.70 5.86 5.86 5.86 4.49 3.13 3.13 2.73 2.73 1.95 17.97	Combat Damage Punctures F.O.D. Denting Combat Damage - Dent F.O.D Punctured Overstress Manuf/Ship/Maint Error	17 12 10 4 3 3 55	3.32 2.34 1.95 0.78 0.59 0.59
* Total forward blade	removals	ls equals 457	7 + 55 = 512		

TABLE XIX,	PERCENT	PERCENTAGES OF AFT	AFT BLADE REMOVALS - CH-47B/C	Ó	
REPAIRED BLADES			SCRAPPED BLADES	ES	
REMOVAL REASON	QTY.	% OF TOTAL REMOVALS *	REMOVAL REASON	QTY.	% OF TOTAL REMOVALS *
F.O.D. Denting Unbonded Boxes F.O.D. Punctures Combat Damage - Punct. Overstress Unbonded (Bulged) Boxes No Valid Removal Reason No Defect (Sched.Maint.) Corrosion Unbonded (Voids) Boxes MWO Compliance Combat Damage - Dents Delaminated (Voids) Remainder	91 335 34 27 26 23 23 11 13 13 430	18.16 7.78 6.99 6.79 5.39 4.39 4.39 2.79 2.79 2.60 1.80	F.O.D. Dented Crashes/Strikes - Minor Damage Combat Damage - Dents Combat Damage - Punct. Internal Discrep. Corr. F.O.D Punctures	23 13 3 3 12 71	4.59 2.60 1.80 1.59 0.60 2.40
* Total aft blade remova	rals equ	equals 430 + 71	= 501 blades		



INHERENT DESCREPANCY-CAUSED REMOVALS - PORWARD BLADES - CH-47 B/C. FIGURE 14.

INHERENT DISCREPANCY OUANTITY



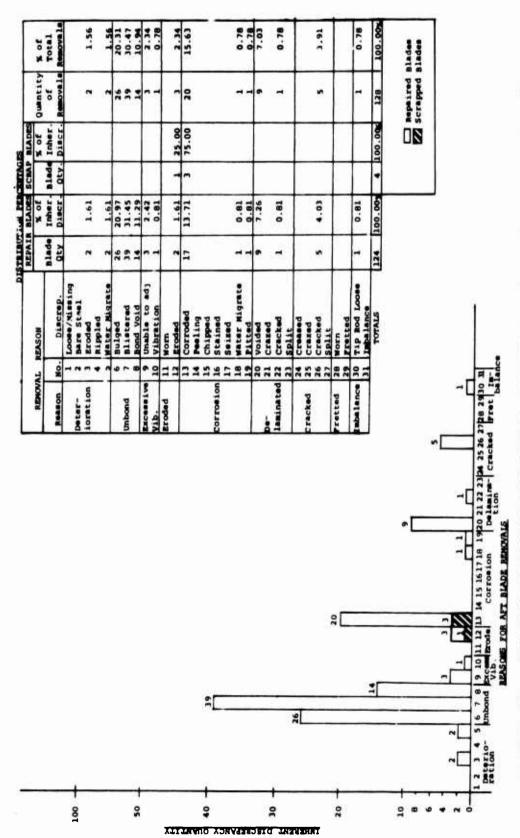
		REPAIR	REPAIRED BLADES SCRAPPED BLADES	SCRAPI	ED BLADES		
4	REMOVAL REASON		10 x		× of		30 %
		Hlade	Blade   Scheduled Blade   Scheduled Rmvl.	Blade	Scheduled	Rmv 1.	Total
on N	Reason No. Discrep.	Oty.	Removals Oty.	Oty.	Removals   Oty.   Removals	Oty.	Removals
	<b>A</b> O	2	5.13			2	5.13
_	Compliance						
Тлпе	2 No Defect	2.3	58.97			23	58.97
.hange	(Scheduled						
-	Maintenance)				_		
	3 Retired Blades	<b>87</b>					
_	4 EIR Engr.	2	5.13			7	5.13
-	Evaluation						
other.	5 No Defect -	10	25.64			10	25.64
_	(To facili-						
	tate maint.)						
-	6 Miscellaneous	7	5.13			2	5.13
	TUTALS	39	100.00%			39	100.00%

FIGURE 16. SCHEDULED REMOVALS - FORWARD BLADES - CH-47 B/C. SCHEDULE REMOVAL REASONS

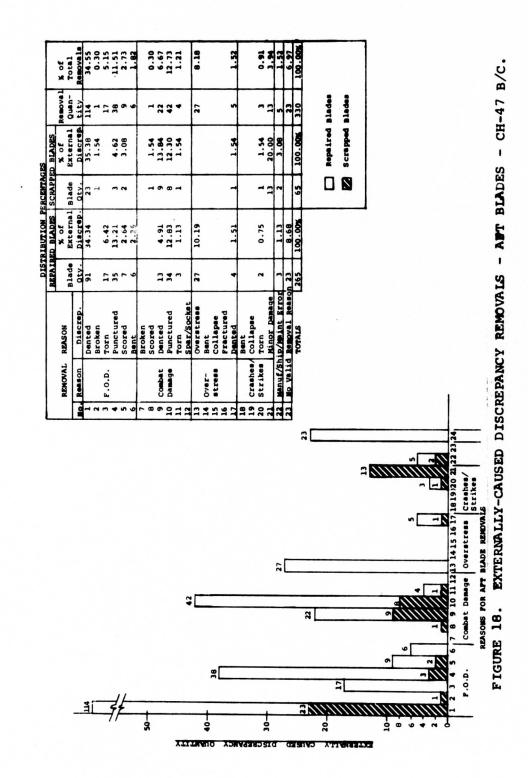
Other

] د

SCHEDATED REMOVES - DISCHEDANCE TANGETTY



INHERENT DISCREPANCY-CAUSED REMOVALS - AFT BLADES - CH-47 B/C. FIGURE 17.



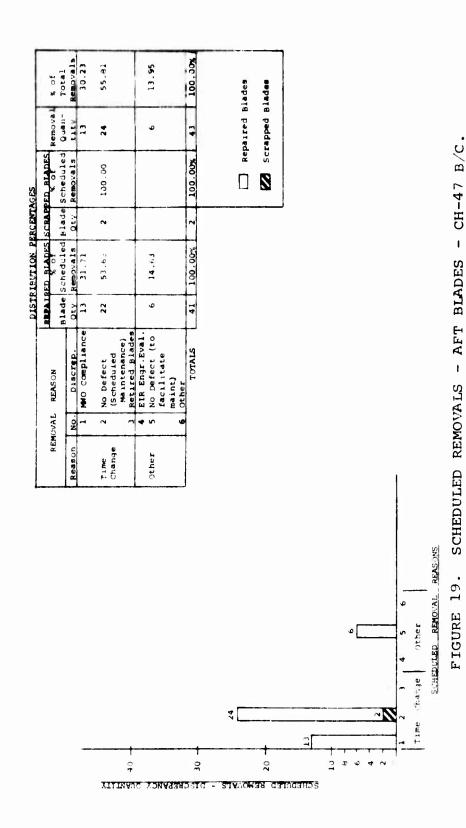


TABLE	E XX.	SUMMARY CH-47B/	٥٥	F PERCENTAGES FORWARD AND A	NTAGE AND	OF FT R	REMOVALS	ALS - BLADES				
		FOR		4	DES *			AFT	ROTOR	R BLADES	+ S	
D M.	Tota Bl	tal – All Blades	Rep B1	Repaired Blades	Scrapp Blade	pbed des	Total Bla	1 - All ades	Repa Bla	ired	Scrapp Blade	p <b>e</b> d les
REMOVAL REASON	Qty.	8	Qty.	о <b>ю</b>	Qty.	οNο	$\mathfrak{o}_{t \mathtt{y}}.$	o40	Qty.		Qty.	1
Deterioration	7	3	2	.3	0	0	4	8.	4	ω,	0	0
Unbonded	65		64		ч	0.19	79	15.77	79	15.77	0	0
Vibration	5	6		6.	0		4	8	4	œ	0	0
Erosion	12	m .		٦.	7	~		9		4.	1	0.20
Corrosion	38	4	37		7		22	۳.	19		٣	9
Delaminated	17	m		٦.	7	-		0		٥.	0	0
Cracked	13	ζ.		٠,	г	7	2	0	S	0	0	0
Fretted	1	4	7	۲.	0	0	0	0	0	0	0	0
Imbalance	m	Ŋ		.5	0	0		.2	1	.2	0	0
F.O.D.	178	4.7		9.	16	H		6.9		7		7
Combat Damage	79	15.43	51	96.6		•	69	13.77	20	96.6	19	3.79
Overstress	36	0		4.	٣	.5		٣.		7	Н	2
Crashes/Strikes	7	۳.	2	۳.	0	0		۲.		4.	14	7
Error	9	٦.	2	.5	٣	0.59	Ŋ	0.	3	9.	2	4
No Valid Reason	16		16		0	0	23	.5	23		0	
O)	0				0	0	0	0	0	0	0	0
Time Change	25	4.88	25	4.88	0	0 0	37	7.38	35	6.99	5	0.40
Other	14	4/	<b>⊣</b>  i	7:1	5		ŀ	1.20		1:1		0.
TOTALS	215	100.00%	457	89.27		10.72	501	100.008	430		7.1	14.16
S	Based	Upon A	ota	Of 51	Ţ	orward B	lade	ស				
	Based	Ø	Total	of 50	1 Aft	$\boldsymbol{\sigma}$	S					

### CH-47B/C Forward and Aft Blades Means Analysis

A series of evaluations of the CH-47B/C rotor blades for their average removal characteristics as based upon frequency of blade removal was accomplished. These calculations of the various removal means followed the approach outlined on pages 20 and 21. Results are given in blade hours.

Tables XXI, XXII and XXIII list the means determined for the major discrepant reasons for removal of the CH-47B/C forward rotor blades. Tables XXIV, XXV and XXVI list similar determinations accomplished for the CH-47B/C aft rotor blades.

Table XXVII presents a summary of the results of these analyses for both CH-47B/C forward and aft blades. This summary may be compared to the CH-47A blade summary shown by Table XVII, on page 40.

	REP	REPAIRED BLADES	S	SCRAF	SCRAPPED BLADES		TOT	TOTAL BLADES	
		Total			Total			Total	
	Qty. of	Fwd. Bld	MTBR	Qty. of	Fwd. Bld.	MTBR	Qty. of	Fwd. Bld.	MIBRE
REASONS FOR REMOVAL	Blades	Flight	•	Blades	Flight	•	Blades	Flight	•
	Removed	Hours		Removed	Hours		Removed	Hours	
Inherent Discrep.	151	-	5,922	5	•	178,867	156	¥	5.733
Deterioration	7		447,169	;	_	:	7		447,169
Unbonded	64		13,974	-		894,339	9		13,759
Excessive Vibration	2	-	178,867	;	_	1	2		178,867
Erosion/Wear	7	894,339	81,304	-	894,339	894,339	12	894,339	74,528
Corroded	37	_	24,171	-	-	894,339	38		23,535
Delamination	16		968'55	-		894,339	17		52 603
Cracked	12		74,528	7		894,339	13		68,795
Fretted	-		894,339	;		!	-		894,339
Imbalance	3	-	298,113	;		-	3	,	298,113
Externally-Caused Discrep.	248	_	3,606	47	-	19,028	295		3,032
Foreign Object Damage	162	-	5,520	16	-	55,896		_	5,024
Combat Damage	51	894, 339	17,536	28	894,339	31,941	79	894,339	11,321
Overstressed	33	_	27,101	٣	_	298,113	36	_	24,843
Crashes/Strikes	2	۰	447,169	:	-	:	2	,	447,169
No Valid Removal Reason	16	894,339	968'55	:	:	;	16	894,339	55,896
Error *	3	894,339	298, 113	3	894,339	298,113	9	894,339	149,056
Scheduled Removals	33	-	22, 932	1	;	1	39	•	22, 932
Time Change	25	894,339	35,774	:	;	;	25	894,339	35,774
Other	14	-	63,881	!	;	:	14	•	63,881
All Causes	457	894,339	1.957	55	894,339	16,260	512	894,339	1.747

MTTRF 458 536 318 396 307 284 TOTAL BLADES Fwd.Bld. Flight 1, 195 4, 916 2, 136 17, 852 13, 852 13, 852 13, 852 202, 775 24,368 1,852 6,259 6,290 112,349 72,580 28,717 5,075 9,857 200 19,266 913 Total Oty. of Blades Removed 156 65 65 12 38 17 295 178 79 36 221 835 349 336 392 543 329 170 624 Manufacturing/shipping/handling error including inadequate field repair. SCRAPPED BLADES Fwd. Bld. Flight 18,423 8,692 9,220 1,874 221 835 349 336 Total 511 22,483 - CH-47 B/C Qty. of Blades MTTRF MEAN-TIME-TO-REMOVAL - FORWARD BLADES REPAIRED BLADES Fwd.Bld. 63,336 999 23,923 1,852 6,038 Flight 4,739 93,926 63,888 19,497 9,346 1,195 4,916 262 17,852 13,396 4,456 5,941 913 18,431 Oty. of Blades Removed 51 Externally-Caused Discrep. Foreign Object Damage No Valid Removal Reason Excessive Vibration REASONS FOR REMOVAL Scheduled Removals Crashes/Strikes Inherent Discrep. Deterioration Combat Damage Erosion/Wear Delamination Overstressed Time Change All Causes TABLE XXII. Imbalance Unbonded Corroded Cracked Fretted Other

	REP	REPAIRED BLADES	SS	SCR	SCRAPPED BLADES	ES	TO	TOTAL BLADES	
		Total			Total			Total	
	Qty. of	Fwd. Bld.	MTBUR	Qty. of	Fwd. Bld.	MTBUR		Qty. of Fwd. Bld.	MTBUR
REASONS FOR REMOVAL	Blades	Flight		Blades	Flight	•	Blades	Flight	
	Removed	Hours		Removed	Hours		Removed	Hours	
Inherent Discrep.	151	*	5,922	5		178,867	156	4	5,733
Deterioration	7		447,169	;		1	7		447,169
Unbonded	64		13,974	-		894,339	9		13,759
Excessive Vibration	2	_	178,867	1	_	!	s		178,867
Erosion/Wear	11	894,339	81,304	7	894,339	894,339	12	894,339	74,528
Corroded	37	_	24,171	7		894.339	38	-	23,535
Delamination	16		968,836	7		894.339	17		52,608
Cracked	12		74,528	7		894,339	13		68,795
Fretted	-		894,339	1		:	-		894,339
Imbalance	3	•	298,113	1	-	-	3		298,113
Externally-Caused Discrep.	248	-	3,606	47	•	19,028	295	•	3,032
Foreign Object Damage	162	894,339	5,520	16	894,339	55,896	178	894,339	5.024
Combat Damage	51	_	17,536	28	_	31,941	79	_	11.321
Overstressed	33		27,101	٣		298,113	36		24 843
Crashes/Strikes	2		447,169	:		;	. 2		447,169
No Valid Removal Reason	16	894,339	55,896	1	:	;	16	894,339	55,896
Error *	3	894,339	298,113	3	894,339	298,113	9	894,339	149,056
All Causes	418	894,339	2,140	55	894,339	16.260	473	894,339	1,891

# Discrepancy Locations Versus Types of Discrepancies

Data included herein has been based upon 'Reasons for Removal' only.

This investigation simplified the amount of data handled by confining the results to major discrepancy locations versus types of inherent discrepancies and to externally-caused discrepancies only.

Figures 20 and 21 demonstrate the results of analyses for inherent and externally-caused discrepancies of the forward blades.

Figures 22 and 23 demonstrate the results of analyses for inherent and externally-caused discrepancies of the aft blades.

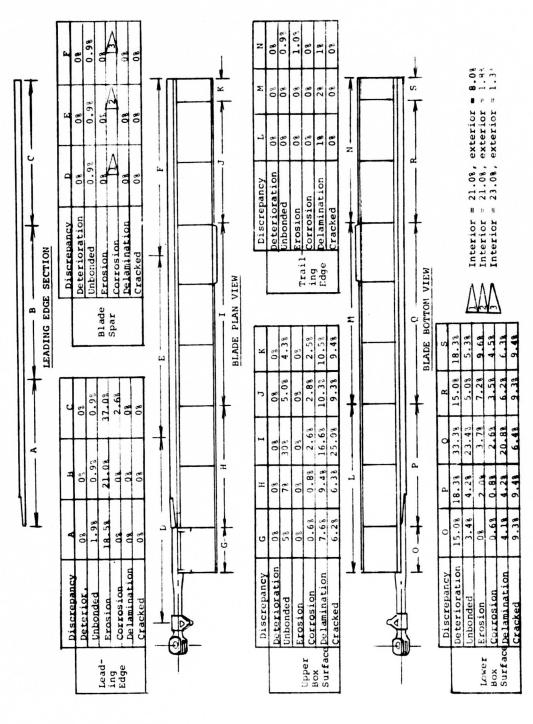
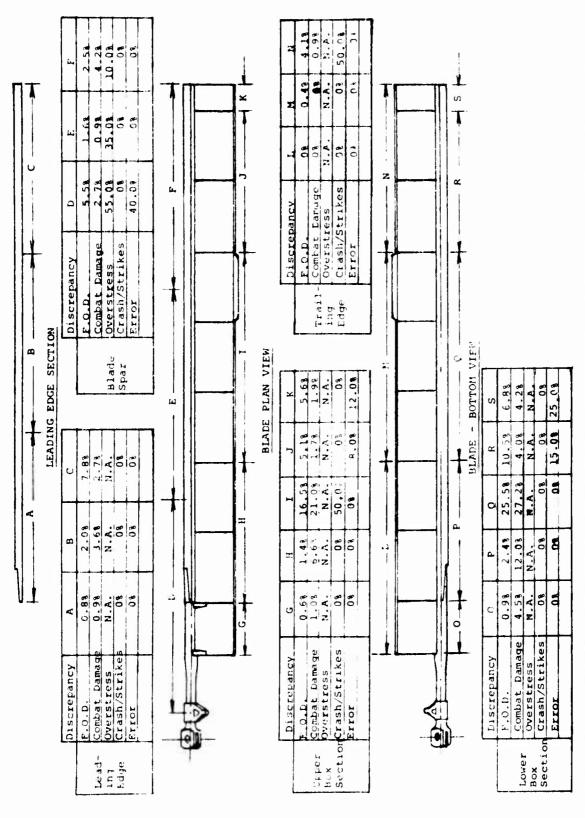
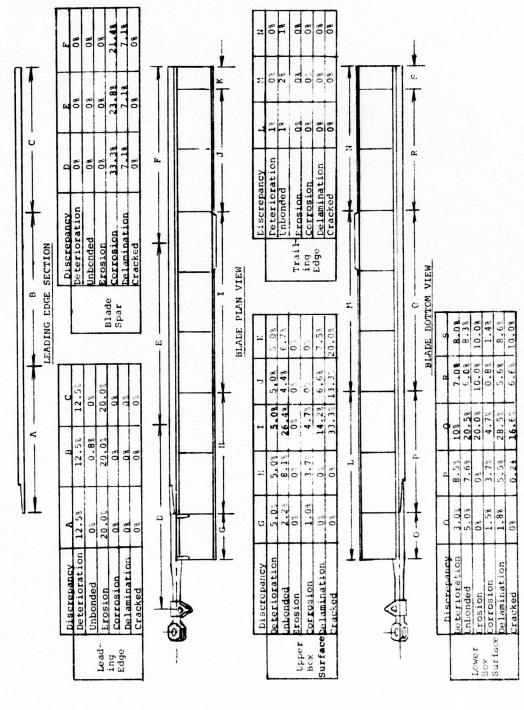


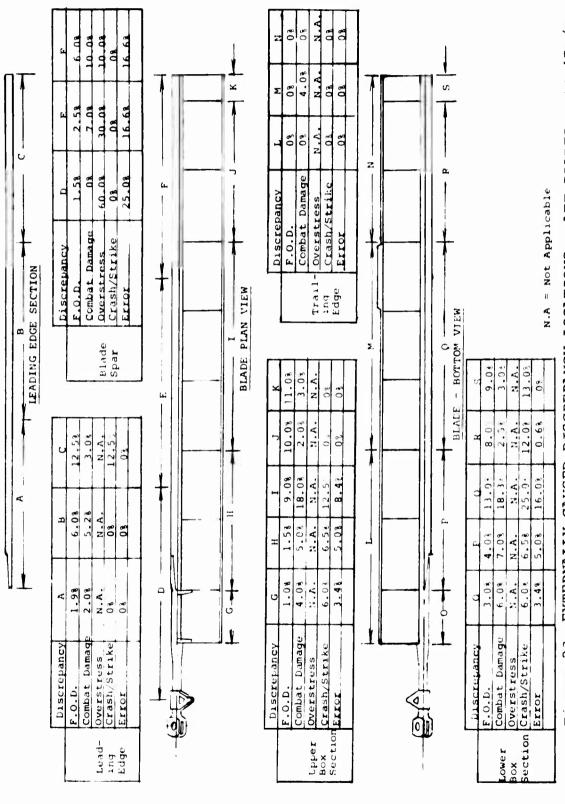
FIGURE 20. INHERENT DISCREPANCY LOCATIONS - FORWARD BLADES - CH-47B/C.



CH-47 B/C. ı - FORWARD BLADES EXTERNALLY-CAUSED DISCREPANCY LOCATIONS 21 FIGURE



INHERENT DISCREPANCY LOCATIONS - AFT BLADES - CH-47 B/C. FIGURE 22.



EXTERNALLY-CAUSED DISCREPANCY LOCATIONS - AFT BLADES - CH-47B/C. 23. Figure

	REPA	REPAIPED BLADES	DES	SCR	SCRAPPED BLADES	ES	TOT	TOTAL BLADES	
		Total			يدا			Ĕ	
REASONS FOR REMOVALS	Qty. of	Aft Bld.	MTBRA	Oty. of	Aft Bld.	MTPR,	0ty. of	Aft Bld.	MTBR.
	Blades	Flight	•	Blades	Flight	•	Blades	Flight	<b>«</b>
	Removed	Hours		Removed	Hours		Removed	Hours	
Inherent Discrep.	124	_	7,128	4	¥	220,956	128		6.905
Deterioration	4	_	220.956	-		!	4		220,956
Unbonded	7.9		11,188	!	-	1	46		11,188
Excessive Vibration	4	_	220,956	!		-	4		220,956
Erosion/Wear	7	883,824	441,912	-	883,824	883,824	m	883.824	294,60e
Corroded	19	_	46.517	m		294,608	22	_	40,174
Delamination	10		88,382	!		1	10		88,382
Cracked	S		176,765	1		-	ß		176,765
Fretted	1		;	!	_	1	}		1
Imbalance	7	-	883,824	1	-	1	7		883.824
Externally-Caused Discrep.	239	•	3,698	63	<b>E</b> -	14,029	302	-	2, 92
Foreign Object Damage	156		5,666	59	-	30,477	185		4.77.
Combat Damage	50	883,824	17,676	19	883,824	46,517	69	883.824	12.80~
Overstressed	31	-	28,510	-1	_	883,824	32	_	27.619
Crashes/Strikes	2	-	441,912	14	-	63,130	16	-	33.23
No Valid Removal Reason	23	883,824	38,427	1		1	23	883. H24	18 427
Error *	m	883,824	294,608	2	883,824	441,912	5	•	176.765
Scheduled Removals	41	•	21,557	7	-	441,912	43	_	20.554
Time Change	35	883,824	25,252	7	883,824	441,912	37	883, 24	23.88°
Other	9	-	147,304	1		1	9		147.304
All Causes	430	883,824	2,055	11	833,824	12,448	501	863,824	1.764

369 415 355 392 466 252 611 223 381 342 342 383 352 316 325 160 472 473 TOTAL BLADES Total Aft Bld. Flight 1,421 30,954 1,863 757 542 103,402 70,433 24,315 6,425 20.279 17.442 2,837 1,909 7,474 2,230 1,229 13,438 185,067 Qty. of Removed Blades 302 185 69 32 16 4 6 4 E 2 5 1 37 8 501 MTTRA 739 356 331 397 433 316 59 391 670 SCRAPPED BLADES Total Aft Bld. Flight 20,876 11,513 8,223 316 554 1,478 1,478 2,401 824 25,309 391 2,010 Hours Qty. of Blades Removed 29 MEAN-TIME-TO-REMOVAL - AFT BLADES - CH-47 B/C MTTRA 345 381 322 213 202 202 325 81 459 456 392 392 466 183 601 223 381 REPAIRED BLADES Aft Bld. Flight 11,428 2,230 1,909 82,526 59,420 16,092 7,474 1,421 18,801 15,964 2,837 1,863 366 609'9 159,758 Total onrs Qty. of Removed Blades 430 239 31 10 Externally-Caused Discrep. Foreign Object Damage No Valid Removal Reason REASONS FOR REMOVAL Excessive Vibration Erosion/Wear Scheduled Removals Crashes/Strikes Inherent Discrep. Combat Damage Deterioration Delamination Overstressed Time Change All Causes TABLE XXV. mbalance Unbonded Corroded Cracked Fretted

\* Manufacturing/shipping/handling error including inadequate field repair

	REPAIRED	TRED BLADES	S	SCR	SCRAPPED BLADES	DES	TO	TOTAL BLADES	3
		Total			Total			Total	
	Qty. of	Aft Bld.	MTBURA	Oty. of	Aft Bld.	MTBUR	Qty. of	Aft Bld.	MTBUR
REASONS FOR REMOVAL	Blades	Flight		Blades	Flight		Blades	Flight	•
	Removed	Hours		Removed	Hours		Removed	Hours	
Inherent Discrep.	124	•	7,128	4	4	220,956	128	*	6.905
Deterioration	4		220,956	;		:	4		220,956
Unbonded	79		11,188	!		!	79		11,188
Excessive Vibration	4		220,956	:		;	4	_	220 956
Erosion/Wear	2	883,824	441,912	7	883,824	883,824	3	883,824	294.608
Corroded	19		46,517	٣	_	294,608	22	-	40 174
Delamination	10		88,382	1		:	10		88.382
Cracked	2		176,765			:	2		176.765
Fretted	1					:	1		;
Imbalance	1	,	883,824	:	>	-	1	*	883,824
Externally-Caused Discrep.	239	-	3,698	63		14,029	302		2,927
Foreign Object Damage	156	883,824	999'5	59	883,824	30,477	185	883,824	4,777
Combat Damage	50	-	17,676	19		46,517	69		12,809
Overstressed	31		28,510	-		883,824	32		27,619
Crashes/Strikes	2	>	441,912	14	>	63,130	16	>	55,239
No Valid Pemoval Reason	23	883,824	38,427	-	883,824	:	23	883,824	38 427
Error *	3	883,824	294,608	2	883,824	441,912	2	883,824	176,765
All Causes	389	883,824	2,272	69	883,824	12,809	458	883,824	1,930

BLADE		COMBINED	INHE PENT DISCREPANCY	EXTERNALLY CAUSED DISCREPANCY	ERROR CAUSED DISCREPANCY	SCHEDULED
MTRR	Scrapped	1,957	5,922	3,606	298,113	22,932
-	Total	1,747	5.733	3,032	149,056	22,932
	Repaired	390	419	379	87	458
MTTRF	Scrapped	409	437	392	624	:
	Total	396	150	381	356	458
	_	2,140	5,922	3,606	298.113	N.A.
MTBURF	0,	16,070	178,867	19,028	298.113	N.A.
	Total	1,891	5,733	3,032	149,056	N.A.
	Repaired	2,055	7,128	3,698	294,608	21,557
MTBRA	Scrapped	12,448	220,956	14,029	441,912	441,912
	Total	1,764	6,905	2,927	176,765	20,554
	Repaired	372	409	345	81	459
MTTRA	Scrapped	356	609	331	277	739
	Total	369	415	342	160	472
		2,272	7,128	3,698	294,608	N.A.
MTBURA	Scrapped	12,809	220,956	14,029	441,912	N.A.
		1,930	6,905	2,927	176,765	N.A.

## CH-47 BLADE SCRAPPAGE ANALYSES

This section of the report includes analyses of the scrappage of the forward and aft rotor blades for both CH-47A and CH-47B/C helicopters.

Analyses concern the following:

- a. Major percentages of blades scrapped
- Quantity of blades scrapped vs. actual reasons for scrappage
- c. Blade teardown experience
- d. Mean-Time-to-Scrappage

The following helicopter blade scrappage analyses have been based upon the known reasons for blade scrappage, not upon reasons for blade removal. Certain blades were removed for reasons other than any known spar damage in the field and returned for inspection and overhaul. Subsequent repair action uncovered spar damage. However, other blades were scrapped, either in the field or immediately upon return inspection without any rework action attempted. In these cases where the reason for scrappage was not given in Boeing-Vertol records, the reason for blade removal was used as the scrappage reason. It may be assumed that reasons for removal may be a good indicator of the reasons for scrappage of blades in the field. Field scrappage reasons and data are not accessible to Boeing-Vertol except through Field Service Representative reports.

Tables XXVIII and XXIX summarize the scrapped blade status for the most frequently occurring causes for scrappage. Table XXVIII concerns the forward blades and Table XXIX concerns the aft blades.

Table XXX, page 77, summarizes the percentages of blade scrappage for CH-47A and CH-47B/C forward and aft blades in terms of reasons for blade scrappage.

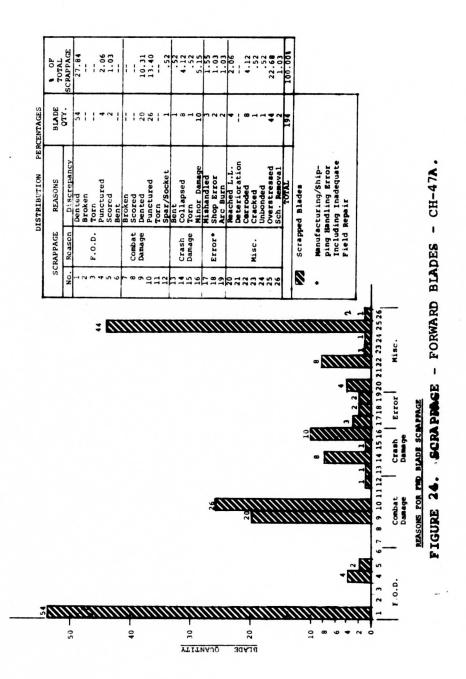
TABLE XXVIII. PERCEN	PERCENTAGES OF	FORWARD BLADE	SCRAPPAGE - CH-47A	AND CH-47B/C	B/C
CH-47A FWD	D BLADES		CH-47B/C FWD	BLADES	
SCRAP DISCREPANCY/ REMOVAL CAUSE	QTY. BLADES	PERCENT OF TOTAL*	SCRAP DISCREPANCY/ REMOVAL CAUSE	QTY. BLADES	PERCENT OF TOTAL +
Dented - F.O.D.  Overstressed Punctured - Combat Damage Dented-Combat Damage Minor Damage-Crashes Collapsed-Crashes Collapsed-Crashes Corroded Punctured - F.O.D. Retired Mishandled - Error Shop Error Arc Burn - Error Scheduled Maint. Scored - F.O.D. Spar/Socket-Combat Damage Bent-Crash Damage Torn-Crash Damage Cracked Unbonded TOTALS:	54 26 20 10 8 8 8 2 2 2 1 1 1 194	7.86 6.40 3.78 2.91 1.46 1.16 1.16 2.29 2.29 2.29 2.29 2.29 2.15 1.5 1.5	Dented - F.O.D. Dented - Combat Damage Punctured - Combat Damage Scored - F.O.D. Dented - Crash Damage Overstressed Punctured - F.O.D. Torn - Combat Damage Torn - Crash Damage Shop Error Arc Burn - Error Corroded TOTALS:	15 14 3 3 1 1 1 55	11.91 11.12 7.94 2.38 2.38 1.59 7.9 7.9 7.9 7.9
* Based upon 687 ( + Based upon 126 (	CH-47A fc	forward and af C forward and	t scrapped blades. Se aft scrapped blades.	Table ee Tabl	XXIX. e XXIX.

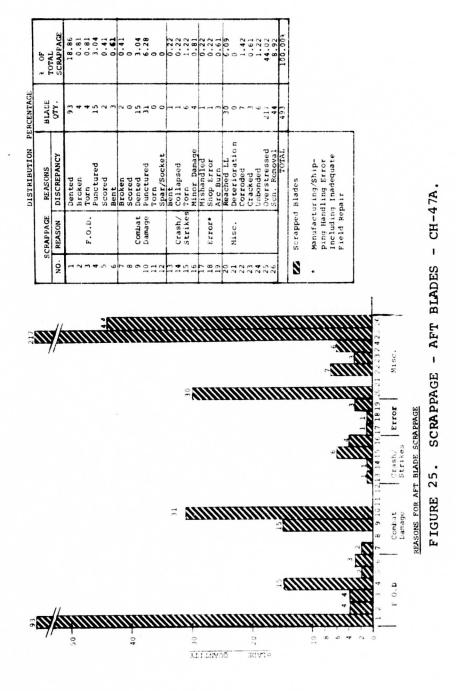
3/C	BLADES	QTY. PERCENT OF TOTAL	23 18.26 13 10.32 9 7.14 8 6.35 3 2.38 3 2.38 1 1.59 1 79 1 779 1 779	Table XXVIII. ee Table XXVIII
SCRAPPAGE - CH-47A AND CH-47B/C	CH-47B/C AFT BI	SCRAP DISCREPANCY/ REMOVAL CAUSE	Dented - F.O.D. Dented - Crash Damage Dented - Combat Damage Dunctured-Combat Damage Overstressed Punctured-F.O.D. Corroded Scored - F.O.D. Mishandled-Error Broken - F.O.D. Scored - Combat Damage Torn-Combat Damage Torn-Crash Damage Torn-Crash Damage	scrapped blades. See ft scrapped blades. S
BLADE		PERCENT OF TOTAL*	31.59 13.54 6.40 4.51 2.18 2.18 1.02 1.02 1.87 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8	and aft ard and a
GES OF AFT	BLADES	QTY. BLADES	217 93 44 31 15 15 66 6 7 7 7 7 7 7 4 4 1 1 1 1 4 9 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	47A for 47 B/C
TABLE XXIX. PERCENTAG	CH-47A AFT	SCRAP DISCREPANCY/ REMOVAL CAUSE	Overstressed Dented - F.O.D. Scheduled Maint. Punctured - Combat Damage Retired Punctured - F.O.D. Dented-Combat Damage Corroded Torn-Crash Damage Unbonded Broken - F.O.D. Torn - F.O.D. Arc Burn - Error Cracked Scored - F.O.D. Broken-Combat Damage Bent - F.O.D. Arc Burn - Error Cracked Scored - F.O.D. Broken-Combat Damage Bent-Crash Damage Collapsed-Crash Damage Mishandled-Error Shop Error	* Based upon 687 CH- + Based upon 126 CH-

The distribution of the percentage of CH-47B/C forward and aft rotor blades that have been scrapped for known causes, either internal or external, is shown in Figures 24, 25, 26 and 27.

Prior to a decision as to the extent of blade damage (including spar damage), the blades may require either a partial or a complete teardown during their repair in Boeing-Vertol shops. A partial teardown consists of the replacement of all blade boxes, the trailing edge and the trim tab. The complete teardown consists of the replacement of all the blade boxes, the trailing edge, the trim tab, and the nose cap, plus any miscellaneous parts, as required. Figure 28 has been provided to indicate the quantity of blades that required either partial or complete teardown versus those blades found unsatisfactory as a result of teardown and therefore scrapped.

Calculation results of mean-time-between-scrappage of forward and aft blades for the CH-47A blades are shown in Table XXXI and for the CH-47B/C in Table XXXII. Table XXXIII summarizes all scrapped blade means.





	1	KEASON	Blade	Total
No.	Reason	Discrep.	oty.	Scrappage
7		Dented	15	27.3
7	F.O.L.	Punctured	7	3.6
3		Scored	3	5.5
4		Dented	14	25.4
2	Compat	Punctured	10	18.2
9	Damage	Torn	1	1.8
7	Crash	Torn	-	1.8
8	Damage	Dented	3	5.5
6		Shop Error	1	1.8
10	Error	Arc Burn	1	1.8
=	4.00	Corroded	1	1.8
12	MISC.	Overstressed	, 3	5.5
		TOTALS	55	100.0%
8		Scrapped Blades		
	Manufa Handli	Manufacturing/Shipping/ Handling Error Including Inadequate Field Repair	. 6	

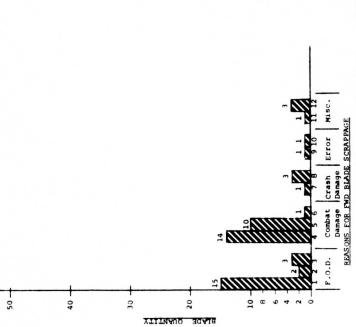
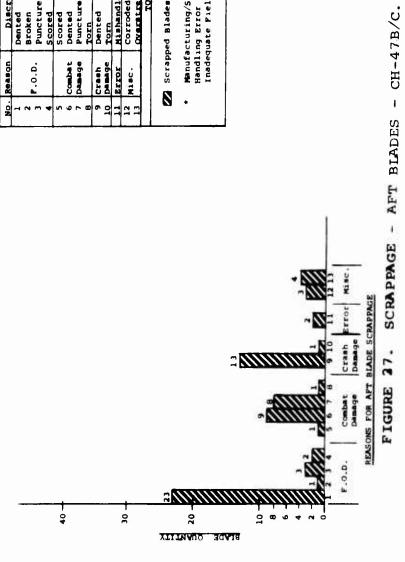


FIGURE 26. SCRAPPAGE - FORWARD BLADES - CH-47B/C.

١		o) believe a second		
Ü	SCRA PDACE	NO STAN		¥ of
3		NO.	Blade	Total
No.	No. Reason	Discrep.	Qty.	Scrappage
4		Dented	23	32.4
~		Broken	-	1.4
~	.0.0.	Punctured	ď	4.2
4		Scored	7	2.8
5		Scored	1	1.4
9	Combat	Dented	6	12.7
7	Damage	Punctured	80	11.3
0		Torn	1	1.4
6	Cresh	Dented	13	18.3
10	Damage	Torn	~	1.4
=	Error	Hishandled	2	2.8
12	MISC.	Corroded	3	4.2
7		Overstressed	+	5.6
Y		TOTALS	7.1	100.0%
0	Scrap	Scrapped Blades		
•	Hanufa Handl Inadec	Manufacturing/Shipping/ Handling Error Including Inadequate Pield Repair	ng/ ding air	
				•



ADE SCRAPPAGE - AND AFT BLADES	SCRAPPED BLADES AFT SCRAPPED BLADES	Quantity   Per	121 24.5	•			3.	•	0	9.7	7		10.3 15 3.0	.4		0.5	10.3	0.5 1 0.	.1 1 0.	.5 6 1.	.2 4	3.6	1.6 1 0.	1	1.0 3 0.	307	30 6.1	-	- E	0.5 6 1.2	7 217 44.	1.0	100.08 493 100.08
PERCENTAGES OF BLADE CH-47B/C FORWARD AND	FORWARD SCR	Quantity	09	54		4		2		47		ć	7.0	56		7	<u>20</u>		8	7	10	7		7		09	<b>4</b>	œ	· ~4	-1	44		194
TABLE XXX. SUMMARY OF PERCE CH-47A AND CH-47	REASONS FOR SCRAP		Foreign Object Damage	Dented	Broken	Torn	Punctured	Scored	Bent	Combat Damage	proveii	Scored	Dented	Punctured	Torn	Spar/Socket	Crash/Strikes	Bent	Collapsed	Torn	Minor Damage	Error	Mishandled	Shop Error	Arc Burn	Miscellaneous	Deterioration	Corroded	Cracked	Unbonded		Scheduled Removal	TOTALS

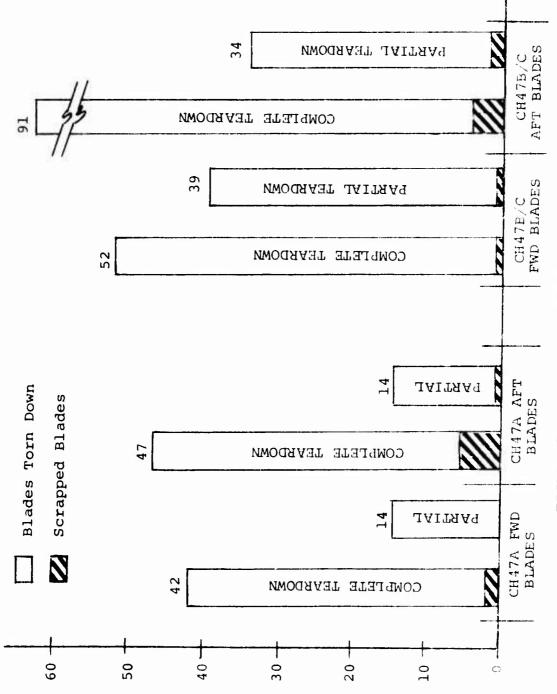


FIGURE 28. BLADE TEARDOWN EXPERIENCE.

	FWD.	SCRAPPED BLADES	ADES	AFT	SCRAPPED BLADES	LADES
REASONS FOR SCRAP	Oty. of Blades Scrapped	Fwd. Blade Flt. Hours	MTBSF	Oty. of Blades Scrapped	Aft Blade Flt. Hours	MTBSF
Foreign Object Damage Dented	54 54	-	32,510	121	-	16,121
Broken Torn		1,950,618		44	1,950,618	487,655
Punctured	7 7		487,655	15 2		130,041
Bent		-		5		650,206
Combat Damage Broken	47	-	41,503	æ þ.		40,638 975,309
Scored	20	1,950,618	97,531	15	1,950,618	130,041
Punctured	26	_	75,023	31	-	62,923
Torn Spa <b>r/Soc</b> ket	-		1,950,618			
Crash/Strikes	<del>0</del> 7	-	97,531	17		162,552
Collapsed	<b>4</b> ∞	1,950,618	243,828		1,950,618	1,950,618
Torn Minor Damage	10		1,950,618	94		325,103
rror •	r 10	019	278,659	<b>1</b> 0 l-	010 030 1	390,124
Shop Error	5 7	7	975,309	• •	10,000,010	1,950,618
Arc Burn	2		975,309	303		650,206
Reached Life Limit	84		487,655		-	65,021
Deterioration	٥	1,950,618	043 626	,	1,950,618	033 656
Cracked			1,950,618	` E		650,206
Unbonded	- 5		1,950,618	91.		325,103
Scheduled Removal	2	>	975,369	44		44,332
Causes	194	1,950,618	10,055	493	1,950,618	

TABLE XXXII. MEAN-TIME-BETWEEN-SCRAPPAGE - FORWARD AND AFT SCRAPPED BLADES - CH-47B/C	EN-SCRAPPAG	E - FORWARD	AND AFT SC	RAPPED BL	NDES - CH-4	7B/C
	FWD.	SCRAPPED BL	BLADES	AFT S	SCRAPPED BLADES	ADES
REASONS FOI SCRAP	Qty. of blades Scrapped	Fwd. Blade Flt.	MTBSF	Oty. of Blades Scrapped	Aft Blade Flt. Hours	MTBSA
Foreign Object Damage Dented	- <del>20</del>	-	\$59,716	29 23	-	30.476
Broken Punctured Scored	3 5	894,339	447,169	- m 2	883,824	294,608 441,912
Combat Damage Scored	25	-	35,774	19		46,517
bented Punctured	10	894,339	63,881	o ∞	883,824	98,203
Torn	7	•	894,339	1		883,824
Crash/Strikes Torn Dented	<b>4</b>   1 ∼	894,339	223,585 894,339 298,113	14 1	852, 824	63,130 883,824 67,986
Error * Mishandled	7	_	447,169	2 <b>1</b> 2	-	441.912
Shop Error Arc Burn		894,339	894,339		883,824	
Miscellaneous Corroded	4 -	894,339	223,585 894,339	r ~	883,824	126,269
Overstressed All Causes	55.3	894,339	298,113 16, <b>26</b> 1	71	883,824	12,448
. * Error Occurred During Manufacturing/Shipping/Maintenance Or Field Repair	facturing/S	ihipping/Mai	ntenance O	r Field Re	pair	

TABLE XXXIII.	KIII. SUMMARY		.47A, B AND	C SCRAPPED	OF CH-47A, B AND C SCRAPPED BLADE MEANS		
BLADES	SS	ALL	FOREIGN OBJECT DAMAGE	COMBAT DAMAGE	CRASHES/ STRIKES	ERROR	MISC.
CH-47A	FORWARD	10,055	32,510	41,503	183,76	278,659	32,150
	AFT	3,957	16,121	40,638	162,552	390,124	6,354
CH-47B	FORWARD	16,261	44,716	35,774	223,585	447,169	223,585
<u> </u>	AFT	12,448	30,476	46,517	63,130	441,912	126,260
					W. C.		

#### COST ANALYSIS

A comparison of the CH-47 rotor blade acquisition cost and the average cost of repaired/reworked rotor blades was made. Included in the total average cost of the repaired/reworked blades is a \$40.00 transportation cost to and from New Cumberland Army Depot (NCAD).

Table XXXVI of Appendix I identifies the various CH-47A (114R1002) and CH-47B/C (114R1502) blades by part number and location. The table shows a selected quantity of blades, transportation costs to and from NCAD, the average repair/rework costs per blade, and the acquisition costs per blade.

The cost comparison of the repair/rework average costs per blade versus the acquisition cost of a new blade is given by this table in percentages.

TABLE XX	TABLE XXXIII. SUMMARY		47A, B AND	C SCRAPPED	OF CH-47A, B AND C SCRAPPED BLADE MEANS		
BLADES	Si	ALL	FOREIGN OBJECT DAMAGE	COMBAT DAMAGE	CRASHES/ STRIKES	ERROR	MISC.
CH-478	FORWARD	10,055	32,510	41,503	97,531	278,659	32,150
	AFT	3,957	16,121	40,638	162,552	390,124	6,354
CH-47B	FORWARD	16,261	44,716	35,774	223,585	447,169	223,585
; ;	AFT	12,448	30,476	46,517	63,130	441,912	126,260
						Control of the second s	

#### CONCLUSIONS AND RECOMMENDATIONS

Removal summaries for all CH-47A blades are given by Table XXXIV and for all CH-47 B/C blades by Table XXXV. As a result of review of these tables and the entire study, the following conclusions and recommendations are made:

- Existing field repair techniques, criteria and/or practices for bonded rotor blades may be inadequate. The detailed data used for this study can be utilized to determine where the inadequacies occur. Recommendations for cost-effective improvements to repair techniques, equipment, procedures and personnel training can be made on the basis of these determinations.
- Trend curves showing the rate of improvement of mean-time parameters for early CH-47A blades through the latest CH-47B/C blades can be derived from the data bank used for this study. Design recommendations based on information extracted and analyzed from the present data bank could lead to improved blade configurations.
- 3. This analysis indicates that returned blades intended for repair/overhaul are being retired or scrapped at periods somewhat less than published life limits. This requires a consideration of acquisition costs in comparison to repair costs and the life remaining in the blade. However, at present, a definitive cost/break-even scale is not available to guide this early retirement practice. Data extracted for this study can be utilized to develop an optimum life limit/repair costs scale for aiding the decision to retire late-life blades.
- 4. The quantity of blades needed to provide a representative sample for meaningful analyses is presently unknown. The CH-47A blade data should be analyzed in smaller groups by manufacturing date and compared to the total results to determine the number required for a representative sample. The CH-47B/C blade analysis should be continued until a representative sample is completed.
- 5. To provide a calendar year analysis of blade discrepancies, the present data should be related to blade manufacturing and repair dates and a yearly updating of the overhaul/repair data should be performed.

_			Lave Rote	r Blades	Art Boto	or Blades	All	Blades
	REMOVAL	REASON	Total	Of	Total	l of	Total	1 of
			Blades	Total	Blades	Total	Blades	Potal
		Loose/Missing	14	0.66		0.04	15	0.34
	Deterior.	Bare Steel Eroded	1 14	0.05	18	0.77	19 29	0.4
	De Callor.	Rippled	1 1	0.14	1 4	0.17	1 "7	0.16
		Water Migrate	lí	0.05	-	1	i	0.02
		Bulged	6	0.20	2	0.09	8	0.1
	Unbond	Blistered	1	0.05	1		1	0.02
S	Vibration	Bond Void Beyond Tolerance	122	5.74	144	6,13	266	5.94
SCREPANCIES	VIDIACION	Vibration	8	0.38	2	0.09	10	0.22
¥	Eroded	Worn	54	2.54	+	0.30	63	1.40
Ž		Eroded	18	0.85	9	0.38	27	0.60
귎		Corroded	141	6.63	99	4.22	240	5.36
၁		Peeling						1
ä	Comment ==	Chipped		1	10	0.42	10	0.22
	Corresion	Stained Seized	2	0.09	1	C.04	1 3	0.07
ż		Water Migrate	•	1 0.09	•	0.04	'	1 0.0
HERENT		Pitted		I	1	0.04	1	0.02
ΗE		Voided	40	1.98	11	0.47	51	1.14
ž		Crazed	2	0.03	1	0.04	3	0.07
_	Delam.	Cracked	5	0.24	23	0.98	25	0.63
	ļ	Split Creased	1	0.05	+ 14	0.81	15	0.43
	Cracked	Crazed	2	0.09		0.00	1 2	0.04
		Cracked	195	9.17	338	14.39	533	11.91
		Split	2	0.09	10	0.42	12	0.27
	Fretted	Worn			11	0.04	1	0.02
	Balance	Fretted Tip Rod Loose	36	0.05	<del>                                     </del>	0.12	40	0.02
	PETEUCA	Imbalance	15	0.70		0.17	19	0.43
	SUBTO		692	32.55	741	31.54	1433	32.02
		Dented	384	18.06	343	14.60	727	16.25
		Broken	14	14 0.66 14 0.66 35 1.65 23 5.78	25	1.06	39	0.87
DISCREPANCIES	F.O.D.	Torn Punctured	35 123		100	1.40	68 223	1.52
		Scored	54		48	2.04	102	2.28
		Bent	38	1.79	27	1.15	65	1.45
		Broken	1	0.19	8	0.34	12	0.27
	Combat	Scored					100	
	Damage	Dented	34	1.60	34	1.45	68	1.52
		Punctured Torn	106	4.98	98	4.30	204	4.56
		Spar/Socket	2	0.09			2	0.04
		Overstress	mi	5.22	279	11.88	390	8.72
	Over-	Bent			1	0.04	1	0.02
	stress	Collapsed				1	,	1
		Fractured	1	0.05	2	0.00	3	0.04
įŀ		Dented Bent	<u>i</u>	0.05	+ 1	0.09	3	0.07
TERNA	Crashes/	Collapse	è	0.38	l i	0.04	9	0.20
١	Strikes	Torn	i	0.05	11	0.47	12	0.27
EXTE		Minor Damage	25	1.17	8	0.34	33	0.74
Ţ	Manuf/Ship/Handling Error No Valid Removal		33 15	1.55	11	0.47	45	1.00
-	No Valid Re	MOV#1	12	0.70	28	0.13	43	0.96
1	SUBTOT		991	46.61	1064	45.29	2055	45.92
1	MWO Complia		32	1.50	35	1.49	67	1.50
- 1	No Defect (	Sch. Maint.)	276	12.98	399	16.99	675	15.08
	Retired Bla		4	0.19	26	1.11	30	0.67
اء	EIR Enginee	ring	2	0.09	2 2 2	0.94	80	0.09
S	N- D-						. 40	1.79
DISCH.	No Defect (	Fac. Maint.)	5 <b>8</b>	2.73				
DISCH.	No Defect ( Miscellaneo SUBTOT	us	71 443	3.34	60 544	2.55	131	2.93 22.06 100.00

			Forward Ro	tor Blades	Aft Rote		All B	
	REMOVAL RE	ASON	Total Blades	% of Total	Total Blades	% of Total	Total Blades	% O
-	· ·	Loose/Missing	112040		D1-44	1000	A A STATE OF THE S	1
		Bare Steel	1					i
	Deterior.	Eroded	1	0.19	2	0.40	3	0.30
		Rippled			١.			
		Water Migr.	30	0.19 5.86	26	0.40 5.19	56	5.5
	Unbonded	Bulged Blistered	16	3.13	39	7.78	55	5.4
	0.20	Bond Void	19	3.71	14	2.79	33	3.20
	Vibration	Beyond Tolerance			3	0.60	3	0.3
•	L	Vibration	5	0.97		0.20		0.5
	Eroded	Worn	5	0.97	,	0.40	5	0.9
ĕ		Eroded Corroded	$\frac{7}{31}$	1.37 6.05	20	4.00	10 31	5.0
<u>.</u>	Corresion	Peeling	31	0.03	1 **	1.00	7.	3.0
ü		Chipped	1 1		1	1 1		!
Discrepancies		Stained	1 1			Ì		İ
ч	!	Seized						
į		Water Migr.	3	0.58	1	0.20	4	0.3
Inherent		Pitted Voided	4 3	0.78	9	0.20	12	1.1
Š	Delam.	Crazed	6	1.17	,	1.73	6	0.5
	223,	Cracked	1	0.58	1	0.20	4	0.3
		Split	5	0.97			5	0.4
		Creased	3	0.58			3	0.3
	Cracked	Crazed	10	1 05	5	1.00	15	1.4
		Cracked Split	10	1.95	,	1.00	13	
	Fretted	Worn		<del></del>		† — †		
		Fretted	1 1	0.19			_1	0.10
	Imbalance	Tip Rod Loome			1	0.20	1	0.10
	CURMOMATE	Imbalance	156	0.58	128	25.55	284	28.04
-	Dented Broken Torn		118	30.40 23.04	114	22.75	232	22.90
			1 1	0.19	1	0.20	2	0.2
	F.O.D.	Torn	13	2.54	17	3.39	30	2.9
		Punctured	34	6.64	38	7.58	72	7.1
		Scored	4	0.78	9	1.79	13	1.20
_	<u> </u>	Bent	<del>-   8</del>	1.56	6	1.20	14	1.30
9		Broken Scored	1 3	0.19 0.58	1	0.20	1 4	0.10
ĕ	Combat	Dented	24	4.69	22	4.34	46	4.54
Ž,	Damage	Punctured	47	9.18	42	8.18	89	8.70
Discrepancies		Torn	2	0.39	4	0.40	6	0.59
•		Spar/Socket	2	0.39		<del></del>	2	0.20
		Overstress Bent	32	6.26 0.19	27	5.39	59 1	5.82
	Over-	Collapsed	1	0.19			•	0.10
	stress	Fractured						
1		Dented	3	0.58	5	1.00	8	0.75
GENAL			1	0.19			1	0.10
External		Bent	_			1	3	0.34
	Crashes/	Collapse	1			0 40		0.30
External	Crashes/ Strikes	Collapse Torn		0.19	3 13	2.59		1.36
		Collapse Torn Minor Damage	1 6	0.19	3 13 5	0.60 2.59 1.00	14 11	
	Strikes Manuf/Ship/Hai No Valid Remov	Collapse Torn Minor Damage nd. Error val Reason	1		13	2,59	14	1.09
	Strikes  Manuf/Ship/Hai No Valid Removation	Collapse Torn Minor Damage nd. Error val Reason	1 6 16	1.17	13 5 23	2,59 1.00 4.59	14 11 39	1.09 3.89
	Strikes Manuf/Ship/Har No Valid Remov Miscellaneous SUBTOTALS	Collapse Torn Minor Damage nd. Error val Reason	1 6 16	1.17 3.13 61.86	13 5 23 330	2,59 1.00 4.59 65.87	14 11 39	1.09 3.89 63.80
<u>.                                      </u>	Strikes  Manuf/Ship/Hai No valid Removi Miccellaneous SUBTOTALS  MMO Compliance	Collapse Torn Minor Damage nd. Error val Reason	1 6 16 317 2	1.17 3.13 61.86 0.39	13 5 23 330 13	2,59 1.00 4.59 65.87 2.59	14 11 39 647 15	1.09 3.89  63.86
<u>.                                      </u>	Strikes  Manuf/Ship/Hai No Valid Remoi Miccellaneous SUBTOTALS  MHO Compliance No pefect (Sci	Collapse Torn Minor Damage nd. Error val Reason	1 6 16	1.17 3.13 61.86	13 5 23 330	2,59 1.00 4.59 65.87	14 11 39	1.09 3.89  63.86
	Strikes  Manuf/Ship/Hai No Valid Remot Miscellaneous SUBTOTALS MHO Compliance No Defect (Sch	Collapse Torn Minor Damage nd. Error val Reason  a. Maint.)	1 6 16 317 2	1.17 3.13 61.86 0.39	13 5 23 330 13	2,59 1.00 4.59 65.87 2.59	14 11 39 647 15	1.00 3.89  63.86 1.41 4.66
-	Strikes  Manuf/Ship/Hai No Valid Remoi Miccellaneous SUBTOTALS  MHO Compliance No pefect (Sci	Collapse Torn Minor Damage nd. Error val Reason	1 6 16 317 2 23	1.17 3.13 61.86 0.39 4.49	13 5 23 330 13	2,59 1.00 4.59 65.87 2.59	14 11 39 647 15 47	1.09 3.89 63.86 1.46 4.64
	Strikes  Manuf/Ship/Hai No valid Remou Micellaneous SUBTOTALS MHO Compliance No Defect (Scl Retired Blades EIR Engineers	Collapse Torn Minor Damage nd. Error val Reason  n.Maint.) s ng	1 6 16 317 2 23 2	1.17 3.13 61.86 0.39 4.49	13 5 23 330 13 24	2,59 1.00 4.59 65.87 2.59 4.79	14 11 39 647 15 47	1.38 1.09 3.85  63.86 4.64 0.20 1.58 0.20 8.10

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## APPENDIX I COST ANALYSIS

The objective of this cost analysis was to analyze the aircraft support costs for rotor blades to determine the average comparative costs of new versus repair/rework blades.

Table XXXVI is provided to indicate results of this analysis.

TABLE XXXVI. COS	r comparis	COST COMPARISON - CH-47 NEW VS. REPAIR/REWORK BLADES	S. REPAIR/RE	WORK BLADES	
Component	Qty. Sample Blades	Transportation To & From NCAD	Total Aver.Costs Per Blade	Acquisition Cost Per Blade	Repair/Rework vs. New
Fwd. Rotor Blade (114R1002)	939	\$40.00/Blade	\$2,808	\$13,200	21.38
Aft Rotor Blade (114R1002)	919	\$40.00/Blade	\$2,416	\$13,200	18.3%
Fwd. and Aft Blade Avg. (114R1002)	1,858	\$40.00/Blade	\$2,614	\$13,200	19.8%
Fwd. Rotor Blade (114R1502)	106	\$40.00/Blade	\$2,175	\$13,800	15.8%
Aft Rotor Blade (114R1502)	09	\$40.00/Blade	\$2,413	\$13,800	17.58
Fwd. and Aft Blade Avg. (114R1502)	166	\$40.00/Blade	\$2,261	\$13,800	16.4%
These costs do not include which are GFE. Costs were completed government delive July 1967 through March 197		s do not include replacement parts GFE. Costs were derived from government delivery orders from through March 1971.	v,		

# APPENDIX II DATA EXTRACTION PROCESS

A data extraction procedure was developed and applied to locate, extract and describe CH-47 rotor blade discrepancies investigated for the purposes of this report. This was done by using an alphanumeric coding system, expanded to accommodate identification of discrepancies within the entire structure of the CH-47 rotor blade. This alphanumeric system provides different codings for the CH-47A and CH-47B/C blades.

Each rotor blade returned to Vertol for repair is treated as if it were appearing in the overhaul system for the first time. A thorough inspection of the blade is made by the Quality Assurance Department. The results of this inspection, including follow-up inspection, are recorded on a Boeing-Vertol Inspection Report throughout the repair/ overhaul process. Each rotor blade assembly upon receipt at Boeing-Vertol is usually accompanied by a Form DA-2410 originated and completed per Army Equipment Record Procedures, TM 38-750, Reference (8), by the using activity. This form will contain blade historical data. An internally originated SAV-HQ Form 391 (Component Disassembly Evaluation Summary) is also completed for contract purposes. Accuracy of subsequent data analysis is dependent upon the accuracy of these documents, as well as the experience of the reviewer of these forms.

The data extraction record devised for this study is comprised of three sheets containing historical data and primary and secondary discrepancy areas of interest under investigation. The sample forms shown are typical of analysis of CH-47A blades. Figure 29 contains historical and chronological data obtained and/or derived from SAV-HQ Form 391 and Form DA-2410. Figures 30 and 31 identify major and minor discrepancy areas in respect to the blade structure. Boeing-Vertol part numbers are included for identification purposes. Thus, a considerable amount of practical information concerning the effect of design, manufacture and operational experience of each rotor blade in the field is extracted in a readily available form. Figures 33 through 40 demonstrate the alphanumeric coding system for the CH-47A blades. A similar system was developed and employed for the CH-47B/C blades.

A concise description of the construction of the data recording sheets, Figures 29, 30 and 31, is given below to illustrate the depth of the data extraction process. Starting with Sheet 1 of the 3-sheet Data Extraction Record (Figure 29), the headings are largely self-explanatory, but the following is provided to indicate consistency of data interpretation:

- 1. Item No. Necessary only for arithmetical continuity and identification of the blade being analyzed.
- Serial No. Serial number of blade being analyzed.
   A-1 indicates blades located on forward rotor head.
   A-2 indicates blades located on aft rotor head.
- 3. Dash No. Indicates changes to basic configuration of blade at arrival (I) and when shipped out of Boeing-Vertol repair/overhaul activity (0).

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- 4. TT Total flight time on blade upon arrival at Boeing-Vertol. Time is obtained from DA-2410 and/or SAV-HQ Form 391 or Boeing Inspection Report. The DA-2410 form from the User Activity is the primary source of this information.
- 5. TSLR Time since last repair which is determined from blade historical records and/or noted on DA-2410. Since each blade is considered new when shipped to Customer after repair/overhaul, this can be considered flight time since last repair.
- 6. Previous Repairs Number of times blade has been repaired/overhauled at Boeing-Vertol before.
- 7. Life Limit Total number of hours blade may be used under normal operating conditions without spar overstress condition. Appears in overhaul and retirement schedule of TM 55-1520-227-20-1 (Reference 6) for CH-47B/C blades. The life limit is fixed at 2400 for the aft CH-47A blades and 3600 for the forward CH-47A blades.
- 8. Date Received Julian date blade is received at repair/overhaul facility.
- 9. Failure Code Major discrepancy noted on DA-2410. Should the failure cause noted on DA-2410 be inconsistent with results of inspection as noted in Inspection Report, the obvious cause of failure should be noted under remarks.

মট: FWD WE ROTOR 31ADES Month Feb. Year 1971	MODEL, A/C	A Blade delivered less socket	DA #2410 incomplete	A Complete Teardown - T/E damage	* B/S intermittent skin to rib voids	Box #2, #3, #4, #5, #7, #8, #9		Scrap - Scrapped in field	Insp. did not reveal reason for removal.	Complete teardown for spar insp.	Dented nosecap obvious	
MONENCLATURE:	EAILURE CODE	Uruk 7		Unk 1				540 A	200 A	804 A		
NOVEN	DATE	5033		Unk				6133	6198	1	1-1	
	DATE RECEIVED	5112		0287				NA NA	6252	9139		
	LIFE	3600		3600				NA	3600	3600 9139		
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PART NUMBER:	NO. NO.	-208 19 33		280 -208 33 57 1126			 	'	-210 33 33	-210 3361 724		
NI N		-208		-203		-		-209 33		-210		
PA	IJEW	279		280				281	282	283		

FIGURE 29. DATA EXTRACTION RECORD - SHT. 1 - CH-47A.

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100	Chan	‡	<del> </del>		7	-	ļ		-			-			
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407	uezi.	×N			F_	2283 M B1		+	-	T H	. *	3	3	_	
1	90N 100N	1				_	1418		1507		-	11458	2200		
Serial No.	<	-208			-208				-209	-210		-210			

FIGURE 30. DATA EXTRACTION RECORD - SHT. 2 - CH-47A.

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	#2 (2) (8) (8) (8) (8) (8) (8) (8) (8) (8) (8		1 11.108 B1.108		1 1 789 1107 1106-1108
	202 816 (2)	T803			
	1 - 200- 11		20 927 812		7 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	114 808 #11 89810 BOX	9	14 2215 B546 H356 -562 B567 B567 B551 -568		02 2203
	Basic Box #10	7333 133	1 2214		1 2202 6 1 2202 1 6
.!	84 \$1005 #9		14 2214	$\Box$	64 6 6 1341 64 6 1341 64 6 1341 64 6 1341
	Basions		14 2214 26 2226	++-	22021410 22021410 8410 1334 1356 1356 1356 1356
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	114R1005	2226	2214 22		2202 23
	14R1005	<b>∂</b> 2	2214 22		2202 2
	B4 5007 808	4 10	2214 22 2225 2225 2		2202 2
	14R100E	99	1 2214 2 2226 2	-	2202
	1481005 #2 11481005 #2 11481005 #2		1 2214 2226 22226 2		2202 2
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	erial No. A	-208	-208	-209	-210
	шеті ••••••••••••••••••••••••••••••••••••	279	288	282	283

FIGURE 31. DATA EXTRACTION RECORD - SHT. 3 - CH-47A.

- 10. Model A/C A, B or C aircraft, as applicable.
- 11. Remarks Major discrepancies, dispositions, or actions taken during repair or overhaul should be noted. Notations such as scrap, complete teardown, partial teardown, TBO Sample, ETR Sample including number, are included. If the blade has been shipped to the Customer, an (S) is placed in the remarks column. If a Boroscope inspection has been completed, a (B) is placed in the remarks column.

Sheet 2 of the Data Extraction Record (Figure 30) and Sheet 3 (Figure 31) provided column headings in terms of the various blade major assemblies and/or subassemblies. Physical and/or environmental damage to the blade surfaces and structure as described in the Inspection Report was analyzed in respect to the primary discrepancy which resulted in blade rework and/or scrappage. Codings which were used are described below:

- 1. A major discrepancy which resulted in scrappage of a part or parts and which was also the cause of blade removal from the aircraft was denoted by placing a (1) in the upper left-hand corner of the appropriate line for that blade. Several examples are shown in Figure 30. Subsequent discrepancies also affecting that part are noted in the same column beneath the first entry.
- 2. A major discrepancy which was considered the primary reason for blade scrappage, but not the blade removal reason, was denoted by placing a 'l' similar to point l above. Subsequent discrepancies are noted below this entry.
- 3. A major discrepancy which required rework or overhaul of a part or parts and which was determined as the blade removal cause was denoted by placing a ② in the upper left-hand corner of the appropriate line for that blade. Subsequent discrepancies are noted below this entry.

- 4. Major blade discrepancies were plotted generally in grid form against blade locations as shown by Figures 32 through 40. Different numbers are employed for each different blade location and particular discrepancy. In those cases where the locating grid was inadequate to describe location, an alphabetical prefix was added to the location number. Alpha prefixes used were 'T' for top of blade, 'B' for bottom of blade, 'L' for leading edge, 'I' for spar interior, etc.
- 5. Discrepancies of secondary importance were described by use of a simple alphanumeric code which is part of the Boeing/Vertol CH-47 Overhaul Data Fact Sheet.

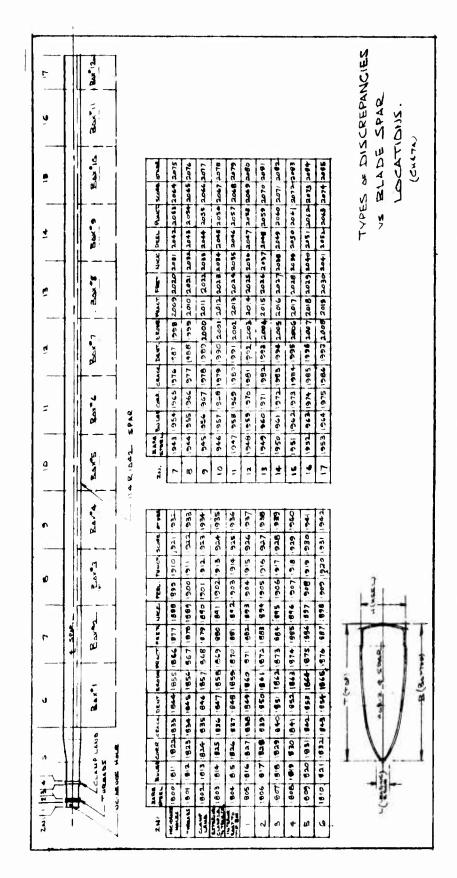


FIGURE 32. ALPHANUMERIC CODE - SHT. 1 - CH-47A.

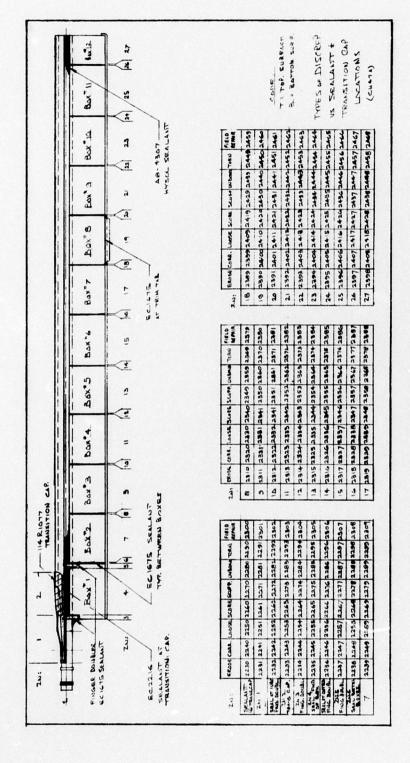


FIGURE 33. ALPHANUMERIC CODE - SHT. 2 - CH-47A.

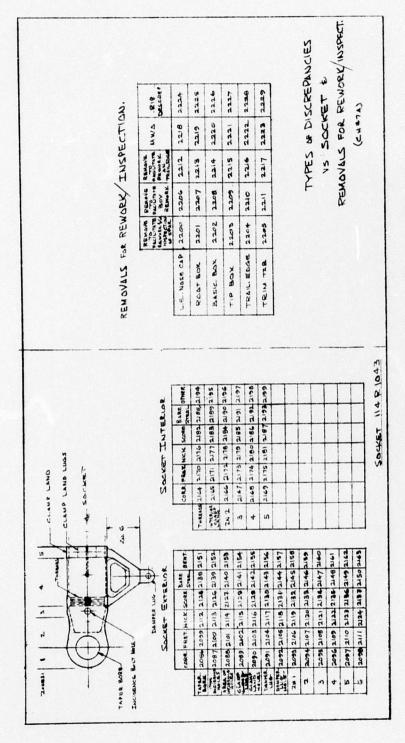


FIGURE 34. ALPHANUMERIC CODE - SHT. 3 - CH-47A.

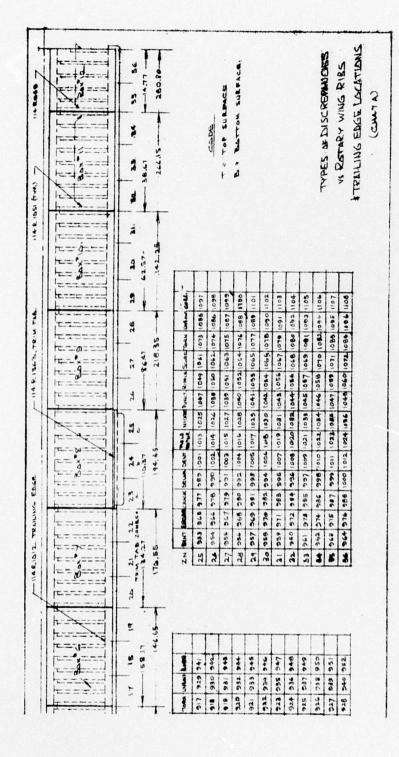


FIGURE 35. ALPHANUMERIC CODE - SHT. 4 - CH-47A.

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FIGURE 36. ALPHANUMERIC CODE - SHT. 5 - CH-47A.

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FIGURE 37. ALPHANUMERIC CODE - SHT. 6 - CH-47A.

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FIGURE 38. ALPHANUMERIC CODE - SHT. 7 - CH-47A.

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FIGURE 39. ALPHANUMERIC CODE - SHT. 8 - CH-47A.

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FIGURE 40. ALPHANUMERIC CODE - SHT. 9 - CH-47A.